

Analysis of Power System Stabilizer Using Fuzzy Logic Controller

Mr. Polamuri Pradeep¹, Mr.N.Vamsi Krishna²

¹*M. Tech Student, ²Assistant professor,*

^{1, 2}*Electrical and Electronics Department,*

^{1, 2}*V R Siddhartha Engineering College, Kanuru*

^{1,2}*Vijayawada, India*

Abstract—The performance of fuzzy-logic power system stabilizer (FPSS), is investigated by applying it to a single-machine power system connected to infinite bus. FPSS is developed using speed deviation and the derivative of speed deviation as the controller input variables. The performance of the system with fuzzy logic based power system stabilizer is compared with the system having conventional power system stabilizer and system without power system stabilizer. The simulation results show that the proposed PSS exhibits very good performance in damping power system low frequency oscillations and greatly improves power system stability.

Keywords: Power system stabilizer, single-machine power system, fuzzy logic control, low frequency oscillations, system stability.

I. INTRODUCTION

The power system is a dynamic system. It is constantly being subjected to disturbances, which cause the generator voltage angle to change. When these disturbances die out, a new acceptable steady state operating condition is reached. It is important that these disturbances do not drive the system to unstable condition.

In the past five decades the PSS have been used to provide the desired system performance under condition that requires stabilization. Stability of synchronous generator depends on a number of factors such as the setting of automatic voltage regulator (AVR). Many generators are designed with high gain, fast acting AVRs to enhance large scale stability to hold the generator in synchronism with the power system during large transient fault conditions. But with the high gain of excitation systems, it can decrease the damping torque of generator. A supplementary excitation controller referred to as PSS have been added to synchronous generator to counteract the effect of high gain AVRs and other sources of negative damping [7].

To provide damping, the stabilizers must produce a component of electrical torque on the rotor which is in phase with speed variations. The application of a PSS to generate a supplementary stabilizing signal, which is applied to the excitation system or control loop of the generating unit to produce a positive damping. The most widely used conventional PSS is the lead-lag PSS, where the gain settings are fixed at certain values which are

determined under particular operating conditions to result in optimal performance for that specific condition. However, they give poor performance under different synchronous generator loading conditions. Conventional PSS (CPSS) is widely used in existing power systems and has made a contribution in enhancing power system dynamic stability. The parameters of CPSS are determined based on a linearized model [2] of the power system around a nominal operating point where they can provide good performance. Since power systems are highly non-linear systems, with configurations and parameters that change with time, the CPSS design based on the linearized model of the power system cannot guarantee its performance in a practical operating environment [3].

II. OVERVIEW OF POWER SYSTEM AND MODELLING

A simplified schematic diagram [3] of a single-machine infinite-bus system is shown in Fig. 1. The system consists of a generating unit connected to a constant voltage bus through two parallel transmission lines. An excitation system and automatic voltage regulator (AVR) are employed to control the terminal voltage, and a governor monitors the shaft frequency and controls mechanical power. Neglecting the transients in the stator circuit and the effect of rotor armature, the synchronous generator can be represented in the form of Park's two-axis machine model by a set of simplified linear equations [2]. The transmission network with an impedance of $r+jx$ is connected to an infinite bus of voltage V_b and the AVR and excitation system are represented by a first-order differential equation. Under normal operating conditions, a linear, time-invariant system can be derived by applying small perturbation relations around a certain equilibrium point. A linearized model is shown in block diagram format in Fig. 2 [6].

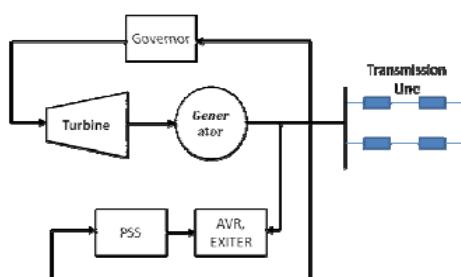


Fig. 1 A schematic diagram of the power system.

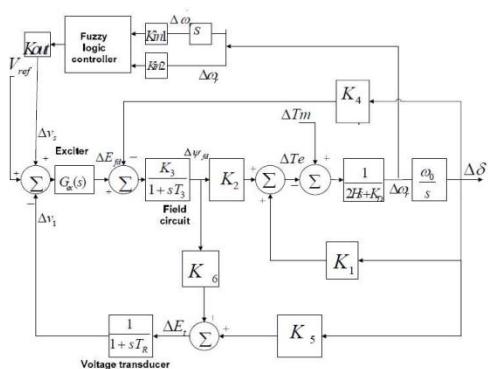


Fig.2 Linearized power system model with FPSS

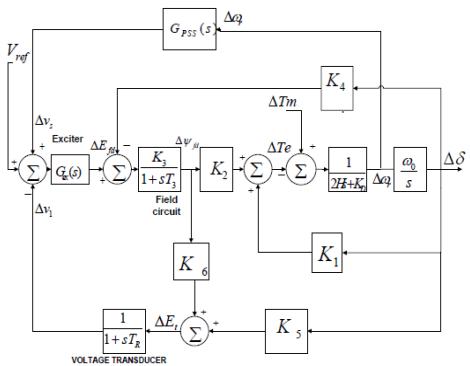


Fig.3 Linearized power system model with PSS

TABLE.1

PARAMETERS
FOR THE LINEARIZED
POWER SYSTEM MODEL

FOR THE LINEARIZED

Parameter	Value
K ₁	1.5495
K ₂	1.2255
K ₃	0.3231
K ₄	0.8910
K ₅	-0.0138
K ₆	0.4942
H	3.5
D	0
T ₃	2.3567
G _a (s)	210
T _R	0.02
ω ₀	314

The block diagram for power system stabilizer [6] is shown below.

TABLE.2

PARAMETERS FOR THE ANALOG PSS

Parameter	Value
T ₁	0.154
T ₂	0.033
T _w	1.4
T _R	0.02
K _{stab}	9.4

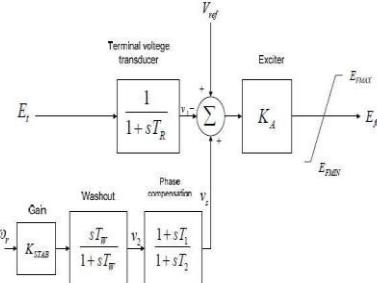


Fig.4 Thermistor excitation systems with AVR and PSS

III.FUZZYLOGICBASEDPSS

The fuzzy control systems are rule-based systems in which a set of fuzzy rules represent a control decision mechanism to adjust the effects of certain system stimuli. With an effective rule base, the fuzzy control systems can replace a skilled human operator. The fuzzy logic controller provides an algorithm which can convert the linguistic control strategy based on expert knowledge into an automatic control strategy. The Fig.5 illustrates the schematic design of a fuzzy logic controller which consists of a fuzzification interface, a knowledge base, decision making logic, and a defuzzification interface.

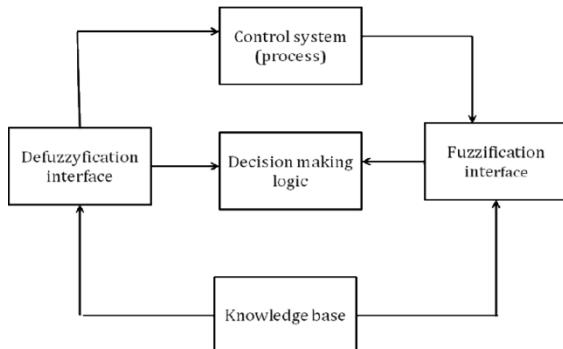


Fig.5 The principle design of fuzzy logic controller

IV.CONTROLLER DESIGN PROCEDURE

The fuzzy logic controller (FLC) design consists of the following steps.

- 1) Identification of input and output variables.
- 2) Construction of control rules.
- 3) Establishing the approach for describing system state in terms of fuzzy sets, i.e. establishing fuzzification method and fuzzy membership functions.
- 4) Selection of the compositional rule of inference.
- 5) Defuzzification method, i.e., transformation of the fuzzy control statement into specific control actions.

MEMBERSHIP FUNCTION:

The variables chosen for this controller are speed deviation, acceleration and voltage. In this, the speed Deviation and acceleration are the input variables and voltage is the output variable.

NB	Negative Big
NM	Negative Medium
NS	Negative Small
ZE	Zero
PS	Positive Small
PM	Positive Medium
PB	Positive Big

Table 3. Membership functions for fuzzy variables.

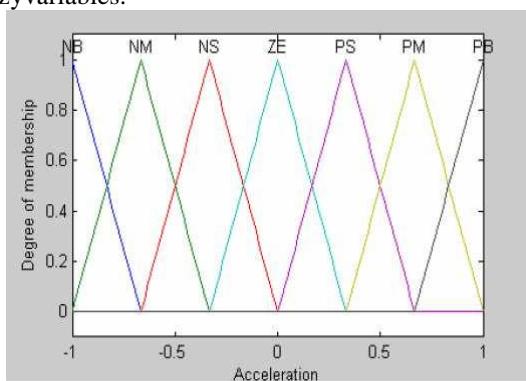


Fig.6 Membership functions for Acceleration

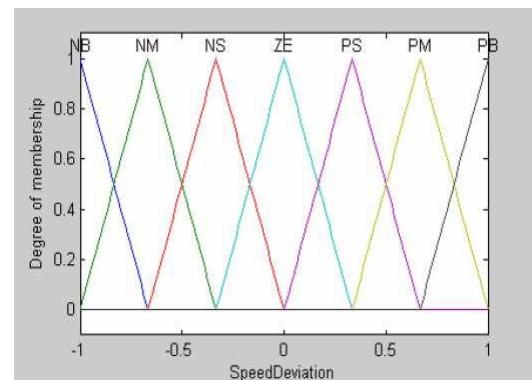


Fig.7 Membership functions for speeddeviation

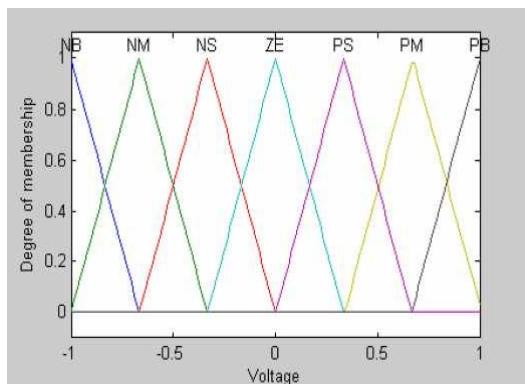


Fig.8 Membership functions for voltage

Each of the input and output fuzzy variables is assigned seven linguistic fuzzy subsets varying from negative big (NB) to positive big (PB). Each subset is associated with a triangular membership function to form a set of seven membership functions for each fuzzy variable. The variables are normalized by multiplying with respective gains $K_{in1}, K_{in2}, K_{out}$ so that their values lie between -1 and 1. The membership functions of the input output variables have 50% overlap between adjacent fuzzy subsets. The membership function for acceleration, speed and voltage are shown below.

FUZZY RULE BASE:

A set of rules which define the relation between the input and output of fuzzy controller can be found using the available knowledge in the area of designing PSS. These rules are defined using the linguistic variables. The two

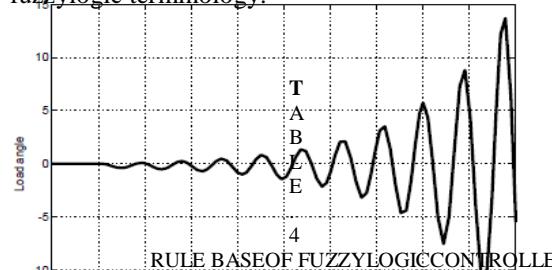
inputs, speed and acceleration, result in 49 rules for each machine. The typical rules are having the following structure:

Rule 1: If speed deviation is NM (negative medium) AND acceleration is PS (positive small) then voltage (output of fuzzy PSS) is NS (negative small).

Rule 2: If speed deviation is NB (negative big) AND acceleration is NB (negative big) then voltage (output of fuzzy PSS) is NB (negative big).

Rule 3: If speed deviation is PS (positive small) AND Acceleration is PS (positive small) then voltage (output of fuzzy PSS) is PS (positive small). And so on....

All the 49 rules governing the mechanism are explained in Table 3.2 where all the symbols are defined in the basic fuzzy logic terminology.



Speed Deviation	Acceleration						
	NB	NM	NS	ZE	PS	PM	PB
NB	NB	NB	NB	NB	NM	NM	NS
NM	NB	NM	NM	NM	NS	NS	ZE
NS	NM	NM	NS	NS	ZE	ZE	PS
ZE	NM	NS	NS	ZE	PS	PS	PM
PS	NS	ZE	ZE	PS	PS	PM	PM
PM	ZE	PS	PS	PM	PM	PM	PB
PB	PS	PM	PM	PB	PB	PB	PB

V.RESULTS AND DISCUSSION

SIMULINK MODEL:

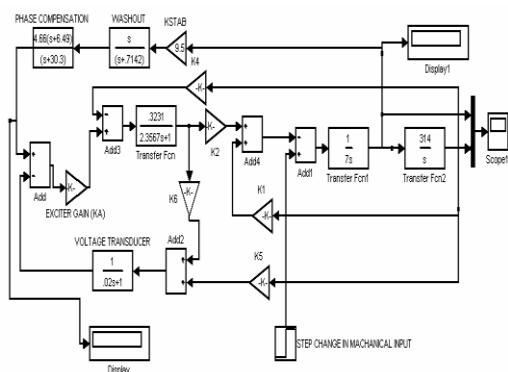


Fig.9 Simulink model connected to infinite bus with PSS for single machine

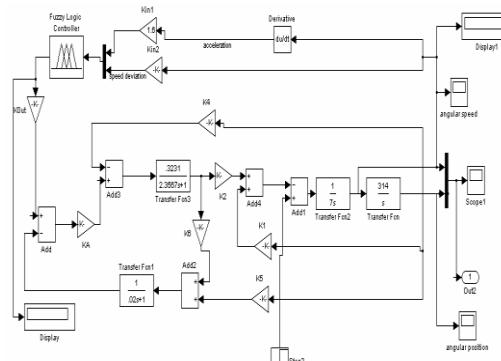


Fig.10 Simulink model for single machine connected to infinite bus without PSS

Case I:

Simulation results without PSS when voltage (0.1 p.u) Disturbance is applied

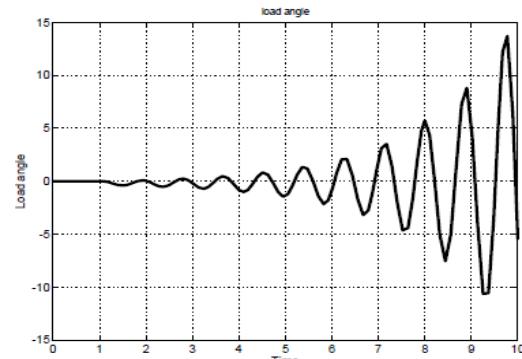


Fig.11 Load angle when 0.1 pp. voltage disturbance applied

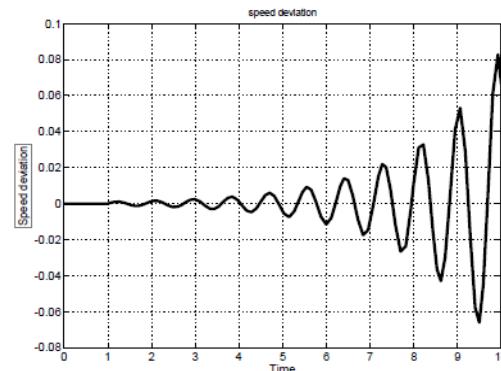


Fig.12 Speed deviation when 5% torque disturbance applied

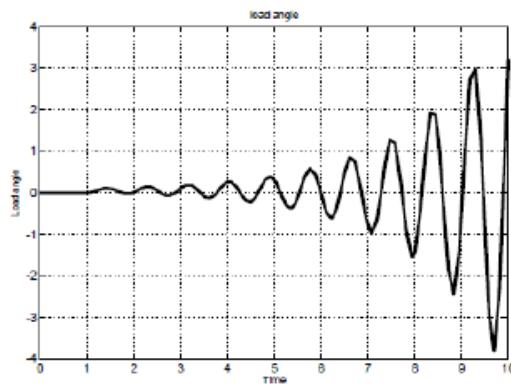


Fig.13 Load angle when 5% torque disturbance applied

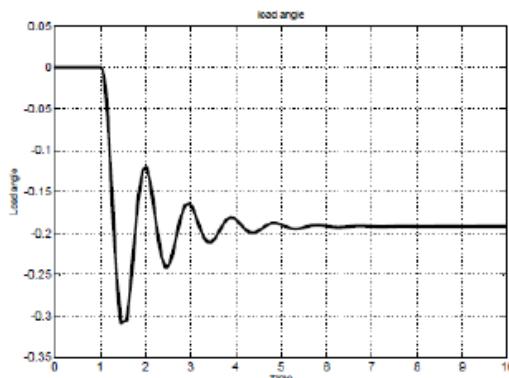


Fig.16 Load angle when 0.1 p.u voltage disturbance applied

CaseII:
 Simulation results with PSS when
 voltage disturbance
 (0.1 p.u) and torque disturbance of 5% is applied.

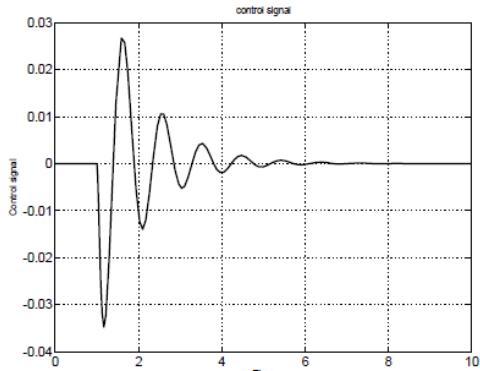


Fig.14 Control signal when 0.1 pp. voltage disturbance applied

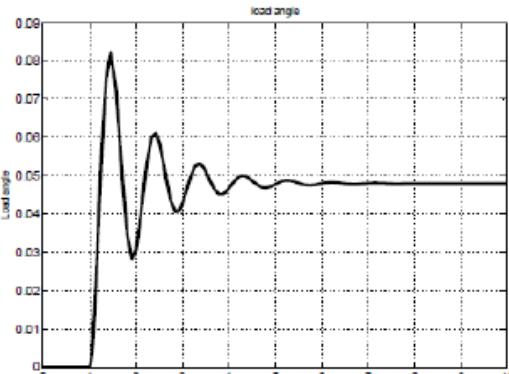


Fig.17 Load angle when 5% torque disturbance applied

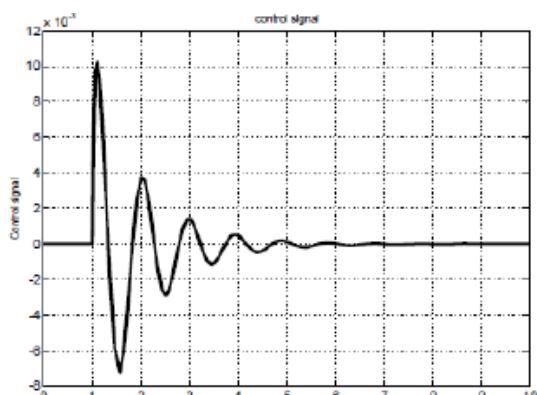


Fig.15 Control signal when 5% torque disturbance applied

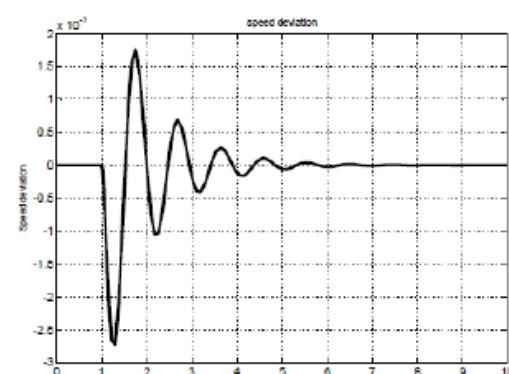


Fig.18 Speed deviation when 0.1 pp. voltage disturbance applied.

CaseIII:
 Simulation results with FPSS when
 voltage disturbance (0.1 p.u) and torque disturbance
 of 5% is applied

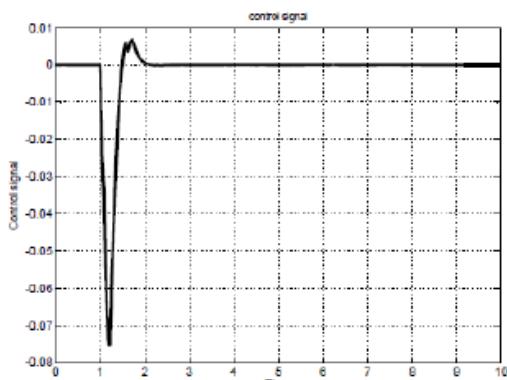


Fig.19 Controlsignalwhen0.1 pp. voltagedisturbanceapplied

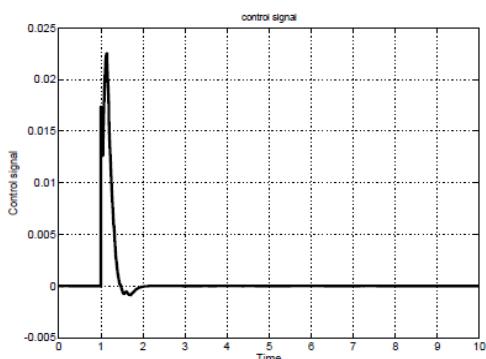


Fig.20 Controlsignalwhen5% torquedisturbanceapplied

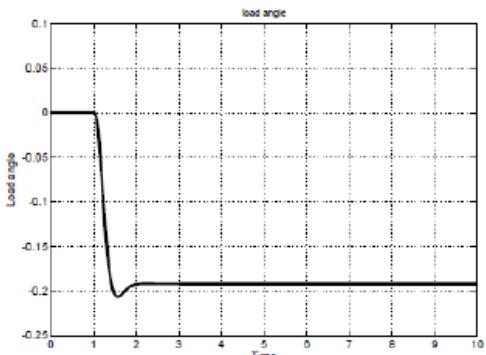


Fig .21 Loadanglewhen0.1 pp.voltagedisturbanceapplied

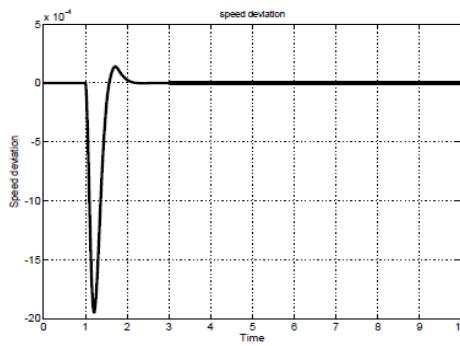
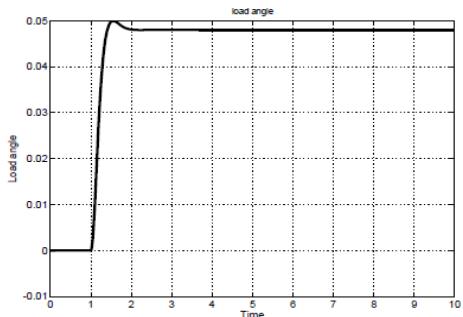


Fig.23 Speeddeviations when0.1 pp.voltagedisturbanceapplied

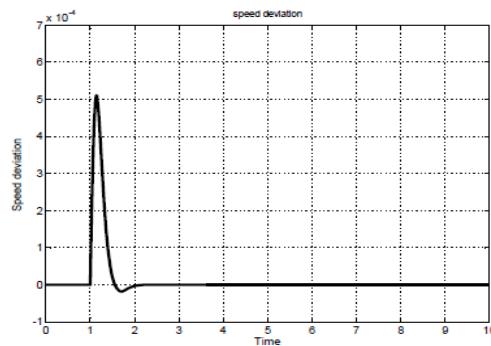


Fig.24 Speeddeviationswhen5% torque disturbanceapplied

VII.CONCLUSION

From the above results we can say that FPSS shows the better control performance than power system stabilizer in terms of settling time and damping effect. It is thus possible to realize the controller efficiently. Therefore, it can be concluded that the performance of the proposed FPSS is much better and the oscillations are damped out much quicker.

REFERENCES

- [1] N.Rafee,T.Chen, and O.P.Malik, "A technique for optimal digital redesign of analog controllers", *IEEE Transactions on Control Systems Technology*, vol. 5, no.1 pp. 89-99, Jan. 1997
- [2] F.P.deMello and Concordia "Concept of synchronous machine Stability as affected by excitation control". *IEEE Transactions on Power Apparatus and Systems*. vol.PAS-88,no.4, 316-329,1969.
- [3] S.Chen, O.P.Malik, "Power system stabilizer design using mu synthesis". *IEEE Transactions on Energy conversion*, vol.10, no.1, 175-181,1996.
- [4] S.Chen and O.P.Malik, "An H-inf optimization based power system stabilizer design". *IEEE proceedings-Generation, Transmission and Distribution*, vol.142, no.2, pp.179-184, 1993.
- [5] HanguShu, "Optimal Design of Multirate Systems". thesis The University of Calgary, April 1997
- [6] P Kundur, "Power System Stability and Control",

- McGraw-Hill 1994
- [7] H.Othman and J.J.Sanchez, M.A.Kale and J.H.Chow, "On the design of robust power system stabilizers", Proceedings of the 28th Conference on Decision and Control .Tampa, Florida December 1989.