

Design and Analysis of Knuckle Joint using AA7075 Material

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ABSTRACT

A knuckle joint is a device used to secure two loaded rods together. When connecting two rods under tensile load, a knuckle joint is utilized. This connection allows the rods to be misaligned in both directions and, with proper guidance, can withstand compressive loads. These joints are employed in the construction of bridges for various kinds of connections, such as tension links and tie rods. One of the rods in this is forked, with eyes at both legs, and the other has an eye at the rod end. A collar and a split pin are used to fasten the pin once it has been placed through the rod end and fork end eyes. In many cases, screwed connections are crucial to the load transmission via machine assemblies. The paper reports on the study and design of a power transmission-related knuckle joint. This study used the Finite Element Method to model and analyse a knuckle joint. Software in three dimensions is used to model the knuckle joint. Modelling in this case was done on CATIA V5. Ansys Workbench 19.0, an analysis program, was used for the simulation portion of the endeavour. The selection of appropriate material, such as AA7075, is necessary to improve operating efficiency. The choice of the most appropriate material for producing the practical knuckle joint is aided by comparing the structural behaviour of the knuckle joints after applying this material to the standard default material that is already in use.

Keywords— ANSYS, FEA, Knuckle joint, Static Structural Analysis

1.INTRODUCTION

A knuckle joint is used to join two rods that are subjected to the action of tensile loads. However, the rods can support compressive loads if the joint is directed. A knuckle joint can be easily disconnected for adjustment or repair. The knuckle joint is used to transmit axial tensile force. A knuckle joint is a mechanical joint that connects two rods or bars at an angle, allowing limited angular movement. It consists of a pin or rod inserted into a series of alternating holes in the two components, enabling rotation and axial movement. Knuckle joints are commonly used in applications where flexibility and articulation are required, such as in linkages and suspension systems. The knuckle joint operates on the principle of a pivot, where the rod end fits between the fork ends, and the knuckle pin passes through aligned holes in both parts. This configuration allows the connected parts to rotate around the pin, providing the necessary angular movement. The figure of a knuckle joint is shown in Fig.1. The knuckle joint assembly consists of following major components.

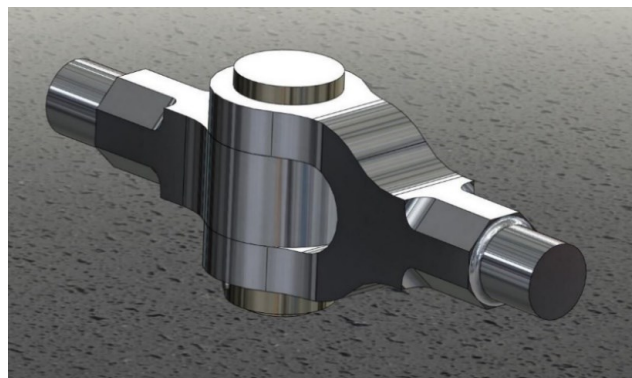


Fig.1 Knuckle joint

- Single-Eye End
- Double-Eye End or Fork End
- Knuckle Pin
- Collar
- Taper Pin or Lock Pin or Split Pin

The picture above displays a knuckle joint in its assembled state. The knuckle pin's axis can be rotated by both the fork end and the eye end in their respective planes.

A knuckle joint may be failed on following three modes. They are:

1. Shear failure of pin (single shear).
2. Crushing of pin against rod.
3. Tensile failure of flat end rod.

The failure of knuckle joint has been studied by several investigators (1-2). Jones (1) has reported that shear failure due to torsional loading is the normal failure mechanism in many engineering components. Pantazopouloes et.al (2) have studied the failure of knuckle joint of a universal coupling system. It was mentioned that torsional overload of a knuckle joint is the major cause of failure. Suraj et.al (3) determines the allowable stress for 30C8 is 400 MPa, and the knuckle joint experiences 201 MPa, ensuring a safe design. A 25 mm pin can support a 50KN load, as confirmed by CATIA modeling and ANSYS analysis. Miss Yogini et al. (4) determined a 30 mm diameter knuckle joint pin made of 30C8 steel was designed to handle a 50KN load. ANSYS analysis with 70,337 nodes and 18,289 elements confirmed the pin's safety with a factor of safety of 5. Theoretical and FEA results closely matched, with maximum tensile stresses and deformation (0.052 mm) occurring in the eye region, highlighting potential crack or fatigue risks.

Ramesh et.al (5) investigated on a knuckle joint made of FE410W material (yield strength 467 MPa) was modeled in SOLID EDGE and analyzed in ANSYS. The analysis showed that a 25 mm diameter knuckle joint can support a load of 229.238KN. Asmaa et.al (6) studied on modified AA7075 alloys were studied during casting and laser melting. AA7075-TiB had the best properties, with finer grains and improved corrosion resistance. AA7075-ScZr also showed better corrosion resistance, while AA7075-standard and AA7075-FeNi had issues with liquation and poor element distribution. Future work will optimize welding and additive manufacturing. K. Emre et.al (7) studied on heat treatment of AA2024 and AA7075 in T3 and T6 was assessed. AA7075-T6 had better strength but lower toughness, while AA2024-T3 showed higher impact energy. AA7075-T6's hardness and strength make it ideal for high-performance applications.

2. THEORETICAL CALCULATIONS

A. Material Selection

Engineers must choose materials that possess the requisite properties for optimal performance, including sufficient tensile strength, yield strength, and hardness to withstand applied loads without deforming or failing. Attributes such as ductility and toughness are also critical, as they enable the material to absorb impact loads and prevent brittle failure, especially in dynamic applications. Furthermore, corrosion resistance is a key factor, particularly in environments exposed to moisture or chemicals, as this property ensures the joint's longevity and reduces degradation risks over time. By carefully considering these material properties, engineers can significantly enhance the reliability and durability of the knuckle joint. There is tensile force applied to the rods. Thus, the criterion for choosing the rod's material is yield strength. Both bending and shear pressures might affect the pin.

Table.1 Material Mechanical Properties

Materials	AA7075-T6	AA7075-Ti+B
Density (kg/m^3)	2810	2810
Youngs Modulus (GPa)	71.7	71.7
Yield strength (MPa)	503	169
Ultimate Tensile Strength (MPa)	572	269
Poisson's Ratio	0.33	0.33

Table .2 chemical composition of wt% of materials

Alloy	Al	Zn	Mg	Cu	Cr	Mn	Ti	B	Fe	Ni	Zr	Sc	Other Elements
AA7075-T6	Bal	5.57	2.38	1.49	0.20	0.03	0.03	-	0.11	-	0.04	-	<0.1
AA7075-TiB	Bal.	6.8	2.2	1.4	0.3	0.3	1	0.2	-	-	-	-	<0.1

B. Selection of factor of safety

In stress analysis of knuckle joint, the effect of stress concentration is neglected. To account for this effect, a higher factor of safety of 4 is assumed in present design.

C. Calculations

$$P = 300 \text{ KN} = 300 \times 10^3$$

Yield strength of material AA7075-Ti + B

$$(S_{yt}) = 169 \text{ N/mm}^2$$

$$\text{Tensile stress } (\sigma_t) = \frac{S_{yt}}{4} = \frac{169}{4} = 42.25 \text{ N/mm}^2$$

$$\frac{S_{yc}}{4} = \frac{169}{4} = 42.25 \text{ N/mm}^2$$

$$\text{Shear stress } (\tau) = \frac{S_{ys}}{fs} = \frac{0.50 S_{yt}}{4} = 67.25 \text{ N/mm}^2$$

Step – i : Dimension of each rod

$$D = \sqrt{\frac{4P}{\pi \sigma_t}}$$

$$= \sqrt{\frac{1200000}{\pi \times 42.25}}$$

$$= \sqrt{\frac{1200000}{132.73}}$$

$$= \sqrt{9040.90}$$

$$= 95.08$$

$$D = 97 \text{ mm}$$

Step – ii : Dimensions of enlarged diameter of each rod by empirical relationship.

$$D1 = 1.1 \times D$$

$$= 1.1 \times 97$$

$$= 106.7$$

$$D1 \approx 108 \text{ mm}$$

Step – iii : Dimension of a & b by empirical relationship.

$$a = 0.75 D$$

$$= 0.75 \times 97$$

$$= 72.75$$

$$a \approx 74 \text{ mm}$$

$$b = 1.25 D$$

$$= 1.25 \times 97$$

$$= 121.25$$

$$b \approx 123 \text{ mm}$$

Step – iv : Dimension of “Pin” a) By shear consideration

$$d = \sqrt{\frac{2P}{\pi t}}$$

$$= \sqrt{\frac{600000}{66.35}}$$

$$\Rightarrow \sqrt{9042.95}$$

$$= 95.04$$

$$d \approx 97\text{mm}$$

b) By bending consideration

$$d_b = \sqrt[3]{\frac{32}{\pi \sigma_t} X \frac{P}{2} \left[\left(\frac{b}{4}\right) + \left(\frac{a}{3}\right) \right]}$$

$$\Rightarrow \sqrt[3]{\frac{32}{132.73} X 150000 \left[\frac{123}{4} + \frac{74}{3} \right]}$$

$$\Rightarrow \sqrt[3]{\frac{32}{132.73} X 150000 \left[\frac{123}{4} + \frac{74}{3} \right]}$$

$$\Rightarrow \sqrt[3]{0.24109 X 150000 X 55.41}$$

$$= 126$$

$$d_b \approx 128\text{mm}$$

The minimum value of diameter of “Pin” (d) = 128

Step – V : Dimension of d_o & d_i by empirical relationship

$$d_o = 2 d \quad d_i = 1.5d$$

$$= 2 \times 128 \quad = 1.5 \times 128$$

$$d_o = 256 \quad d_i = 192$$

Step – vi : Checking the tensile crushing and shear stress in eyes

a) $\sigma_t = P / b(d_o - d_b)$

$$= 300000 / 123(256 - 128)$$

$$\Rightarrow 19.05 < 42.25 \text{ N/mm}^2$$

b) $\sigma_c = P / b(d_b)$

$$= 300000 / 123(128)$$

$$= 300000 / 15744$$

$$\Rightarrow 19.05 < 42.25 \text{ N/mm}^2$$

c) $\tau = P / b(d_o - d_b)$

$$= 300000 / 123(256 - 128)$$

$$= 300000 / 15744$$

$$\Rightarrow 19.05 < 21.25 \text{ N/mm}^2$$

Step – vii: Checking the tensile crushing and shear stress

a) $\sigma_t = P / 2a(d_o - d_b)$

$$= 300000 / 2(74)(256 - 128)$$

$$= 300000 / 18944$$

$$\Rightarrow 15.8365 < 42.25 \text{ N/mm}^2$$

b) $\sigma_c = P / 2a(d_b)$

$$= 300000 / 2(74)(128)$$

$$\Rightarrow 300000 / 18944$$

$$= 15.836$$

c) $\tau = P / 2a(d_o - d_b)$

$$= 300000 / 2(74)(256 - 128)$$

$$= 300000 / 18944$$

$$\tau = 15.836 < 21.12 \text{ N/mm}^2$$

Hence The design is safe

Table.3 Dimensions of knuckle joint

Parameters	Symbols	Values (mm)
Axial load	P	300 KN
Diameter of each rod	D	97
Enlarged diameter of each rod	D ₁	108
Diameter of knuckle pin	d	128
Thickness of each eye of fork	a	74
Thickness of eye end of rod-B	b	123
Outer diameter of eye of fork	d _o	256
Diameter of pin head	d _i	192

3.CAD MODELLING

Making a CAD model is the initial stage in finite element analysis. A 128 mm-diameter knuckle joint that is subjected to tensile force has been examined. The design using the dimensions of the knuckle joint used in this investigation are displayed in Fig. 1. Dimensions displayed in Table.3 are used in CATIA V5 R20 to generate the CAD model of the knuckle joint. The assembled CATIA model of the knuckle joint is displayed in Fig. 2.

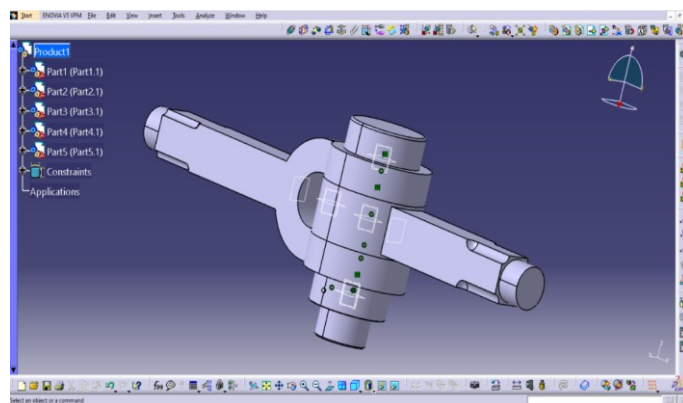


Fig.2 Knuckle joint Model using CATIA

4.STATIC STRUCTURAL ANALYSIS USING ANSYS

For modelling and simulation tasks in complex fields such as advanced engineering manufacturing, transportation, housing, and architectural design, finite element analysis is an essential tool. We consider a knuckle joint with a diameter of 128 mm. An ANSYS 15.0 model is imported once the assembled CATIA model has been converted into STP format. With 135,700 nodes and 103,870 elements, the ANSYS meshed model of the original knuckle joint is displayed in Fig 3.

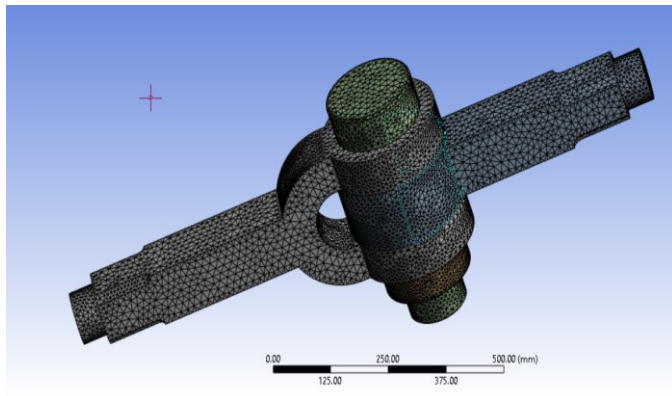


Fig.3 Meshing

5.RESULTS AND DISCUSSIONS

Table.4 shows the results of shear stress and tensile stress for fork, eye and pin by theoretical calculations with their maximum permissible limits when the load is considered as 300KN and the material used is AA7075-Ti+B.

Table .4 Stress calculations by Analytical method

Element	Type of stress	Analytical calculations stress results (N/mm ²)	Maximum Permissible limits (N/mm ²)
Eye	Shear stress	19.05	21.25
	Tensile stress	19.05	42.25
Fork	Shear stress	15.836	21.25
	Tensile stress	15.83	42.25
Pin	Shear stress	21.25	21.25
	Tensile stress	21.25	21.25

a)Static Structural Analysis of Pin

Figure 4 shows the shear stress of Pin, which is 21.25 MPa analytically. This value is confirmed by the FEA result, which is 6.0773 MPa, which is less than maximum stress limit. The pin's normal stress

in Figure 5 is 15.027 MPa, or less than the allowed stress determined by FEA, despite being 21.25 MPa according to

theoretical calculations. Thus, a pin under stress is safe. Figure 6 shows that the highest shear stress for a pin calculated by ANSYS is 17.779 MPa, which is less than 21.25 MPa maximum allowable limit. Therefore, pin is secure.

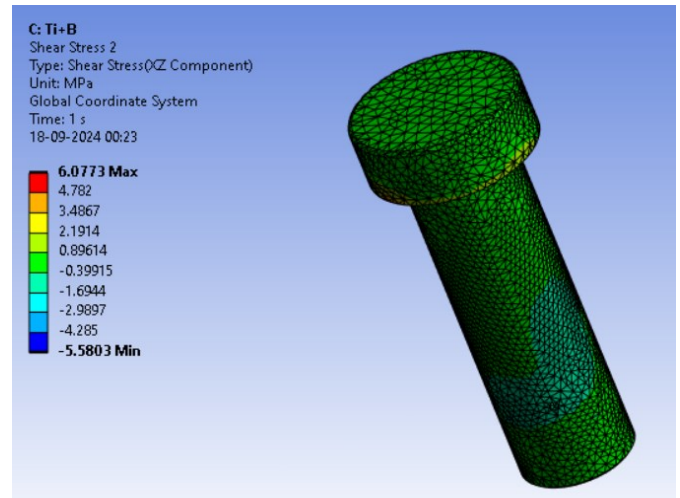


Fig.4 Shear stress for pin using AA7075-Ti+B

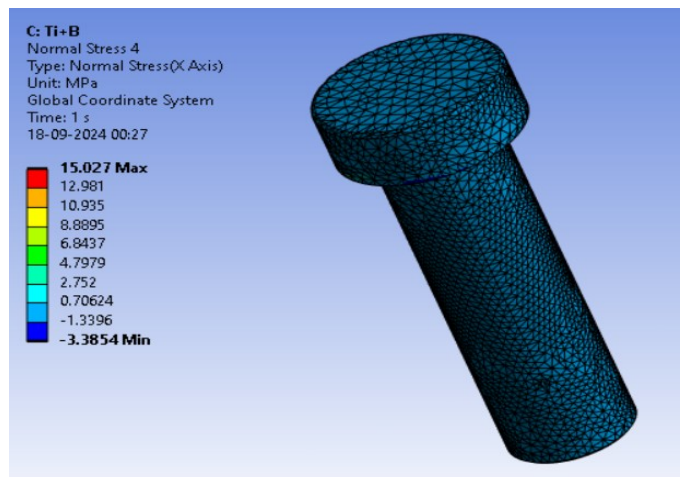


Fig.5 Normal stress for pin using AA7075-Ti+B

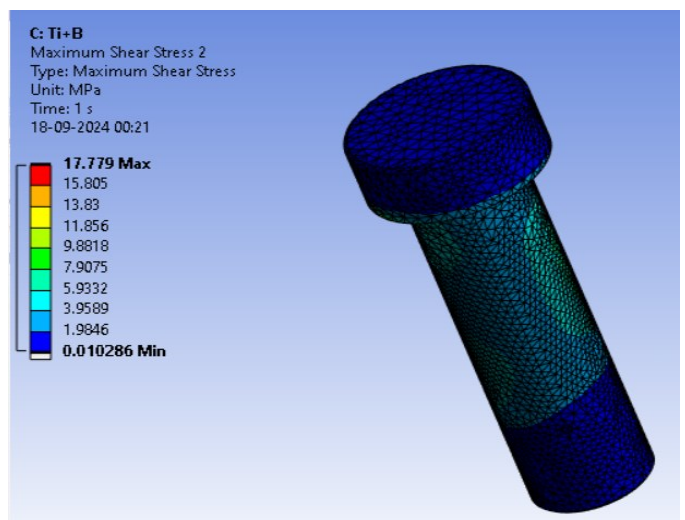


Fig.6 Maximum shear stress for pin using AA7075-Ti+B

b) Static Structural Analysis for Eye

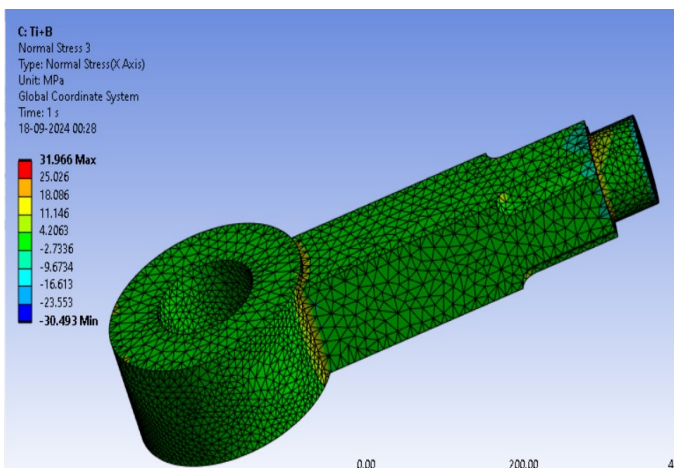


Fig.7 Normal stress for eye using AA7075-Ti+B

c) Static Structural Analysis of Fork

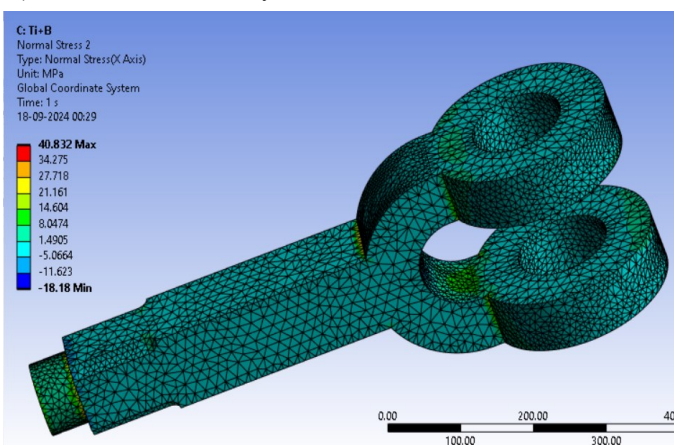


Fig.10 Normal stress for fork using AA7075-Ti+B

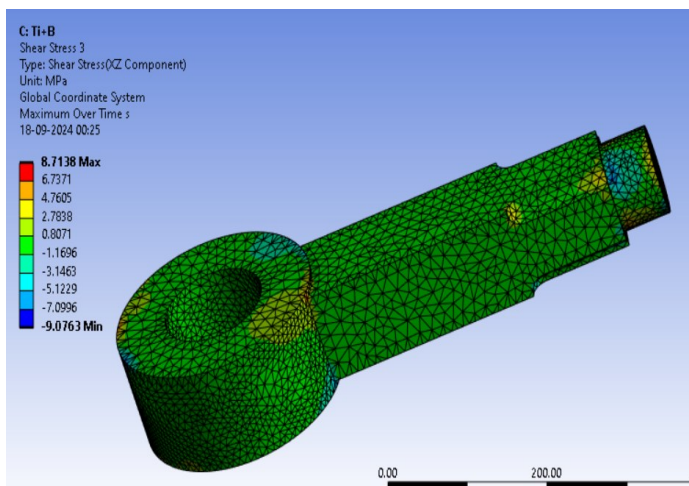


Fig.8 Shear stress for eye using AA7075-Ti+B

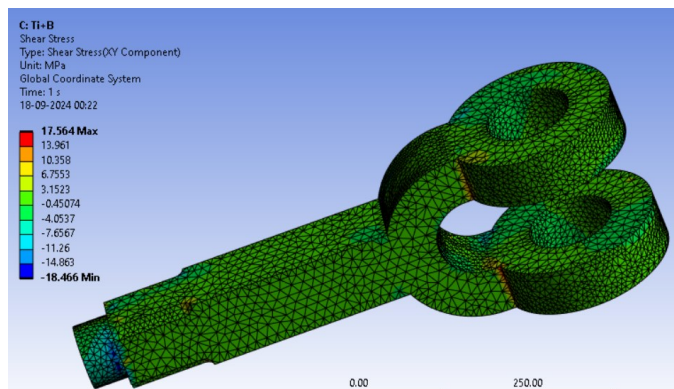


Fig.11 Shear stress for fork using AA7075-Ti+B

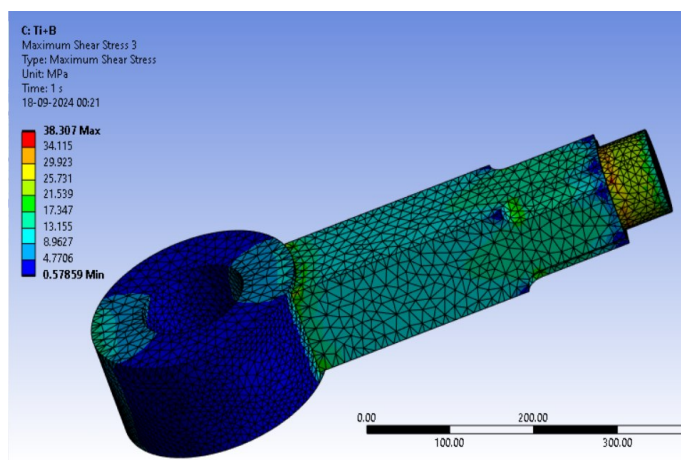


Fig.9 Maximum shear stress for eye using AA7075-Ti+B

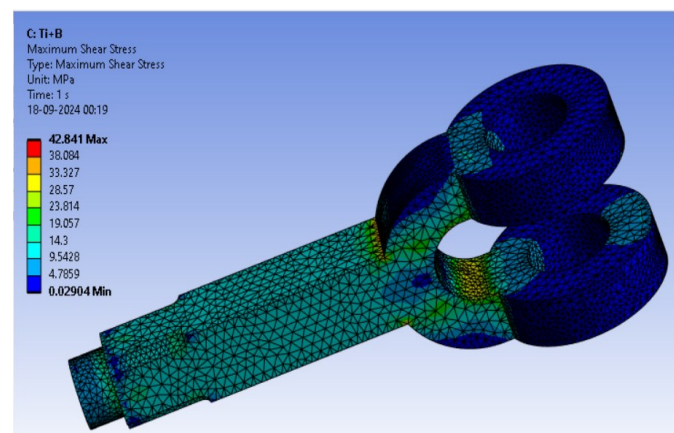


Fig.12 Maximum shear stress for fork using AA7075-Ti+B
 As seen in fig.10 the normal stress for fork by FEA is 40.832 MPa which is less similar to theoretical stress i.e. 15.832 MPa but it is less than maximum permissible limit i.e. 42.25 MPa . Hence fork is safe for tensile stresses. Fig 11 explains, the shear stress for fork by FEA is 17.564 MPa, which is less than to theoretical stress value i.e. 15.832 MPa, and also less than maximum permissible limits i.e. 42.25 MPa. Hence fork is safe for shear stress. Maximum shear stress for fork with 42.841 MPa, as seen in fig.2

In fig.7, the normal stress for eye is 31.966 MPa which is less similar to theoretical normal stress 19.05 MPa, but is below maximum permissible limit. i.e. 42.25 MPa. Hence eye is safe for tensile stress. Fig.8 explains the shear stress for eye by FEA is 8.7138 MPa which is less than theoretical calculations i.e. 21.25 MPa. Hence eye is safe for shear stress. Fig.9 shows the maximum shear stress for eye with 300 KN force, i.e.38.307 MPa.

Table.5 Validation of results

Element	Type of stress	Hand calculations stress results (N/mm ²)	FEA Results (N/mm ²)	Maximum Permissible limits (N/mm ²)
Eye	Shear stress	19.05	8.7138	21.25
	Tensile stress	19.05	31.966	42.25
Fork	Shear stress	15.836	17.564	21.25
	Tensile stress	15.83	40.832	42.25
Pin	Shear stress	21.25	6.0773	21.25
	Tensile stress	21.25	15.027	21.25
	Max. shear stress	21.25	17.779	21.25

Table.5 shows the comparison of shear and tensile/normal stress values for eye, fork and pin by theoretical and FEA method.

d) Static structural analysis of knuckle joint

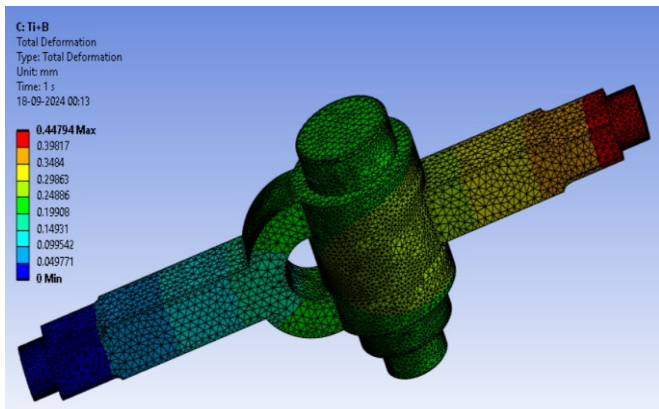


Fig.13 Total Deformation of Knuckle joint using AA7075-Ti+B material

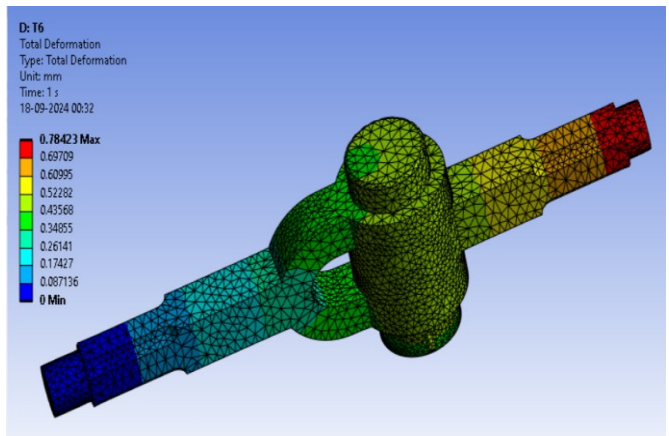


Fig.15 Total Deformation of Knuckle joint using AA7075-T6 material

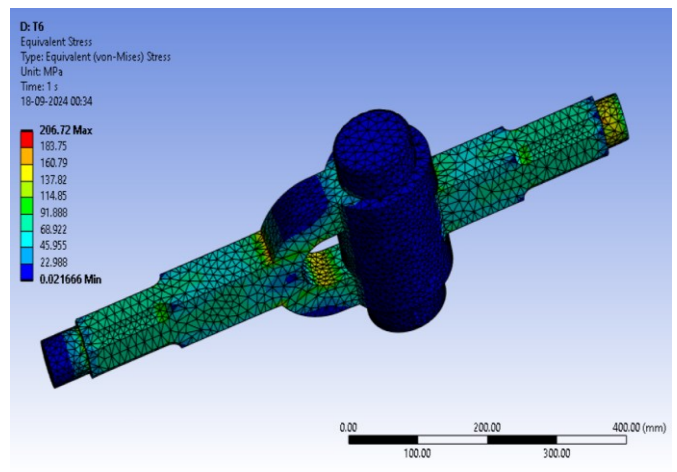


Fig.16 Equivalent Stress of knuckle joint using AA7075-T6 material

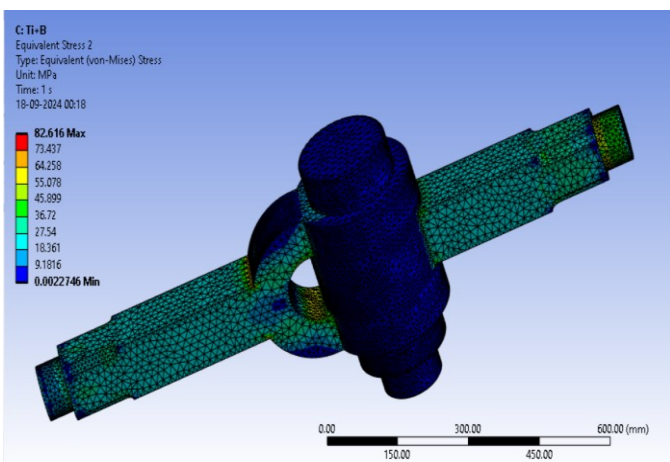


Fig.14 Equivalent Stress of knuckle joint using AA7075-Ti+B material

Table.6 Results comparison chart

Materials	Total Deformation(mm)	Maximum stresses (MPa)
AA7075-Ti+B	0.44794	82.616
AA7075-T6	0.78423	206.72

Table.6 describes the total deformation and maximum stresses obtained when applying tensile load is 300KN using AA7075 but with different chemical composition weight percentages and the results obtained are compared in the above table and found out that when comparing the maximum stress among these two materials, AA7075-Ti+B shows better results because the stresses developing when using this material obtains less stresses when compared with AA7075-T6.

6. CONCLUSION

The knuckle joint being developed in this study is designed to withstand an applied force of 300KN. The diameter of the pin is approximately 128 mm, and the material selected for the knuckle joint is AA7075-T6 and AA7075-Ti+B. A 3D CAD model of the knuckle joint was created based on the calculated dimensions. For the stress analysis, a mesh was generated, comprising 1,35,700 nodes and 1,03,870 elements. The simulation was performed using ANSYS software, producing results including stress contours, tensile stress distribution, displacement contours, and total deformation contours for both the eye pin and the fork.

The ANSYS analysis indicates that a pin with a diameter of 30 mm can safely withstand a load of 300KN when a factor of safety of 4 is applied. The theoretical stress values for shear, tensile, and maximum allowable stresses closely align with the FEA stress results. Since both the theoretical and FEA results are nearly identical and remain below the maximum allowable stress for all components, it can be concluded that the design is safe for all three components. This agreement between the theoretical and FEA results confirms the accuracy of the FEA software. Additionally, it can be concluded that the region of the eye where the 300KN force was applied experiences the highest tensile stresses, as depicted in figure 10.

The analysis shows that the material with a lower yield strength experiences considerably lower stresses compared to the material with higher yield strength under similar loading conditions. This suggests that, although both materials are capable of effective performance, the material with lower yield strength operates in a safer stress range, which may contribute to better ductility and a reduced likelihood of failure. These results imply that the material with higher yield strength is more appropriate for applications requiring greater load-bearing capacity and structural stability. However, when choosing materials for specific uses, it is crucial to also factor in aspects like fatigue performance, toughness, and resistance to corrosion.

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