

GaAs MESFET's Capacitance Model For The Optically Controlled Short-Gate Length Using MATLAB

Sanjay.C.Patil¹, B.K.Mishra²

^{1,2} Department of Electronics and Telecommunication Engineering

¹ Research Scholar at NMIMS (MUMBAI), Parshvanath College of Engineering, THANE (W), MUMBAI, 400601 INDIA

² Thakur College of Engineering and Technology, Kandivali (E) MUMBAI, 400101 INDIA

Abstract: -For GaAs MESFET the capacitance of optically controlled short Gate –length modeled analytically using Gaussian doped channel The photo effects on the short gate-length GaAs MESFET device capacitances have been modeled along with the electrical bias dependencies. The modeling has been done for linear as well as saturation region of device operation. The proposed model has been verified using MATLAB

Key-Words: - Gate-source capacitance, Gate-drain capacitance Vertical Gaussian-Like doping profile, MATLAB

I. INTRODUCTION

The microwave characteristics of GaAs MESFET can be controlled by incident light radiation having photon energy greater or equal to the band gap energy of GaAs in the same manner as varying the gate bias. By biasing the FET optically, many devices such as high-speed optical detector and converter for interaction of optical and microwave signals have been designed.

Optically controlled GaAs MESFET is the considered key device used for the design of photo-detector [1-3]. It is experimentally established fact that optical radiation incident on the transparent or semitransparent gate of the device is used to control the microwave characteristics of the OPFET [4-5]. It has also been investigated that many of the microwave characteristics of GaAs MESFET like resonant frequency, transit time etc., can be controlled by controlling the internal gate-source and gate-drain capacitances of the device [6-7]. Here it is worth mention that the level of incident illumination can change the charge distribution under the gate that determines the internal capacitances of the GaAs MESFET. Therefore the internal capacitances of GaAs MESFET can also be controlled by the incident illumination.

In the conventional microwave amplifiers and oscillators using GaAs MESFETs once the circuit is designed for a certain gain or resonant frequency, it cannot be changed except the value of some of the external component of the circuit is changed. But using optically biased GaAs MESFET provides us with means of one control terminal from which the microwave characteristics of the GaAs MESFET can be controlled by changing its internal capacitances.

A number of capacitance models for long channel optically controlled GaAs MESFET have been described [6, 8-10]. In view of the fact that for high speed and denser integrated circuits the device dimensions are getting smaller and with the reduction in device dimensions two dimensional (2D) effects become prominent. So in order to provide efficient simulations and accurate predictions of photonic microwave integrated system behavior having short gate-length MESFET devices, a careful development of an accurate model taking 2D effects into account is required. Some models for the capacitances of GaAs MESFET are present in the literature [7, 11- 12] that considers two dimensional effects.

For internal capacitances of ion-implanted self-aligned short-channel GaAs MESFETs under dark and illuminated conditions. But that model ignores the effect of sidewall capacitances since the capacitances due to the sidewalls are negligible in self aligned GaAs MESFET device. Sidewall capacitances can play an important role while determining the internal capacitances of non-self aligned GaAs MESFET device. Therefore in the present work we have considered the sidewall capacitances while determining the overall internal capacitances of non-self aligned GaAs MESFET.

The modeling of Gaussian profile introduces the error function which is not fully analytical in nature. The error function is originated because of the non-integrable nature of the Gaussian function over some finite interval. Thus in the present work, an analytic Gaussian-like analytic function proposed by Dasgupta et al. [13] has been used in place of actual Gaussian profile to make the work fully analytical.

II. DEVICE ANALYSIS

The device under consideration has been shown in Fig.(1) where 'a' is the active channel thickness and 'L' is the gate length. Indium Tin Oxide (ITO) has been assumed as the gate metal because of its higher optical transmittance [15]. The monochromatic light is incident on the Schottky gate-metal with photon flux density. The substrate of the device is assumed to be an undoped high pure semi-insulating GaAs material.

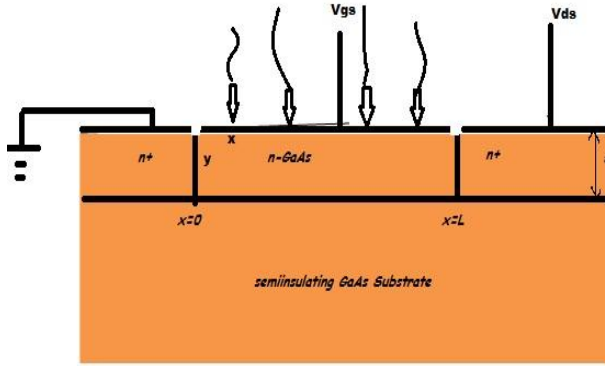


Fig.1.Schematic of GaAs MESFET

The active channel region of the device is an n-GaAs layer which is assumed to be obtained by ion implanting Si into the semi-insulating substrate

The ion distribution profile in the channel region can be given as [15]

$$N(y) = N_p \exp \left[- \left(\frac{y - R_p}{\sigma - \sqrt{2}} \right)^2 \right] - (1)$$

Where R_p is projected range and σ is the projected straggle and $N_p = \frac{Q}{\sigma \sqrt{2\pi}}$ is the peak Ion concentration

in the substrate. Q is the dose The doping concentration in the channel can be given as [17]

$$N_d(y) = N_s + (N_p - N_s)F(y) - (2)$$

Where N_s is the substrate doping concentration and

$$F(y) = \exp \left[- \left(\frac{y - R_p}{\sigma \sqrt{2}} \right)^2 \right]$$

Since $F(y)$ cannot be integrated analytically. We have to use an approximate analytic form of $F(y)$ as [13]

$$F(y) = C_c \left[\left\{ a_c + \frac{2b_c \beta}{\sqrt{2\sigma}} (y - R_p) \right\}^2 - 2b_c \right]$$

$$\exp \left[- \frac{a_c \beta}{\sqrt{2\sigma}} (y - R_p) - \frac{b_c}{2\sigma^2} (y - R_p)^2 \right] - (3)$$

Where $a_c = 1.7857142$, $b_c = 0.6460835$,

$C_c = 0.28\sqrt{\pi}$ and $\beta = \begin{cases} +1 & \text{for } y > R_p \\ -1 & \text{for } y < R_p \end{cases}$

When the light is incident on the gate metal carriers are generated within the semiconductor material. The generated electrons move towards the channel region and holes move towards the surface where they recombine with surface traps. Considering these effects of generation and recombination the net doping concentration can be given as [18]

$$N_D(y) = N_d(y) + G(y)\tau_n - \frac{R\tau_p}{a} - (4)$$

Where $N_d(y)$ represents the doping profile defined by equation (2)

R is the surface recombination rate α is the absorption coefficient of GaAs material

τ_n and τ_p are life time of electron and holes. Respectively

$G(y)$ is the photon generation rate

Under illumination, the optical radiation penetrates into the active layer of the MESFET which results in the generation of the excess electron-hole pairs in the active region of the MESFET. The excess holes generated due to illumination in the depletion region are swept out towards the metal side whereas the photo-generated holes generated in the neutral region are diffused into the depletion region. These excess photo-generated holes in the neutral region as well as in the depletion region are finally swept out towards the metal at the Schottky gate. [10]. This gives rise to a photocurrent flowing from the semiconductor layer into the metal side that develops a photo voltage across the Schottky junction to make the junction forward biased. This photo voltage can be given as [18].

$$V_{op} = \frac{nkT}{q} \ln \left(1 + \frac{J_p(0)}{J_s} \right) - (5)$$

Where J_s is reverse saturation current density at the gate depletion layer interface, n is the ideality factor of the Schottky junction, K is the Boltzmann constant, T is room temperature (i.e., 300K), q is the charge of an electron, and

$J_p(0)$ is the hole current density at the gate-channel interface [18].

III. CAPACITANCE MODELING

We have assumed so far that the depletion region is confined only in the channel region below the Schottky gate and we have computed the 2D potential function accordingly. However, in practice, the depletion region below the gate has a very complicated structure and has extensions towards both the source and drain sides in a very complex manner depending on the bias conditions of the GaAs MESFET [7, 19].

we write

$$L_1 = h(x) : x = 0 - (6)$$

$$L_2 = h(x) : x = L - (7)$$

Where $h(x)$ -is the depletion region height under the gate same as Ref.[12].

The heights of the depletion region in the Regions IV and V can respectively be described as

$$h(x) = \sqrt{L_1^2 - x^2} \quad \text{for } -L_1 < x < 0 - (8)$$

$$h(x) = \sqrt{L_2^2 - x^2} \quad \text{for } -L < x < L + L_2 - (9)$$

It may be noted that the onset of velocity saturation of the electrons has been assumed to be occurred at

$x = L_3 < L$. Thus, the region $L_3 < x < L + L_3$

(i.e. Region II) represents the portion of the saturation region confined below the gate and the region

$$L_3 + L_3 < x < L + (L_3 + L_3) = L_3 + L_3 + L_3 - (15)$$

(Region III) represents the extension of the velocity saturation region beyond the gate with

$L_{sat} = L_3 + L_{ex}$ representing the total length of the velocity saturation region in the channel [20]. The

expressions for the L_3 and L_{ex} can respectively be

given by [20].

$$L_3 = 2.06K_d \left(\frac{\epsilon_s (V_{ds} - V_{sat})}{q\sqrt{n_{cr}N_D(y)}} \right)^{1/2} - (10)$$

$$L_{ex} = 2.06(1 - K_d) \left(\frac{\epsilon_s (V_{ds} - V_{sat})}{q\sqrt{n_{cr}N_D(y)}} \right)^{1/2} - (11)$$

where K_d is a domain parameter, n_{cr} is the characteristic

doping density of GaAs (typically $n_{cr} = 3 \times 10^{21} / m^3$)

and V_{sat} is the minimum drain-source voltage required for

the onset of velocity saturation given as[22].Following the same assumption of linear region the lengths of depletion region extensions towards source and drain in saturation region can be given as

$$L_4 = h(x)_{sat} : x = 0 - (12)$$

$$L_5 = h(x)_{sat} : x = L - (13)$$

Where $h(x)_{sat}$ is the depletion region height under the gate in saturation region same as Ref.[19]. The depletion region heights are given as

$$h(x)_{sat} = \sqrt{L_4^2 - x^2} \quad \text{for } L_4 < x < 0 - (14)$$

$$h(x)_{sat} = \sqrt{L_5^2 - (x - L)^2} \quad \text{for } L < x < L$$

Now, the gate-source and gate-drain capacitances of the GaAs OPFETs can be defined as [7]

$$C_{gs} = \frac{\partial Q_t}{\partial V_s} : V_{gd} = \text{constant} - (16)$$

$$C_{gd} = \frac{\partial Q_t}{\partial V_{ds}} : V_{gs} = \text{constant} - (17)$$

Where Q_t is the total charge in the depletion under the gate of the device. Since depletion region charges are different for linear and saturation region due to the different structures of depletion region.

The total charge Q_t in the depletion region under the linear region of operation of the device can be obtained by the addition of the charges contained in region I, IV, V respectively. The charge in various regions of depletion can be evaluated using following relation [7]

$$Q = qZ \int N_D(h(x)) dx dh(x) - (18)$$

$$\text{and } Q_t = Q_a + Q_b - (19)$$

Where Q_a and Q_b are

$$Q_a = qZ[L_1[K_1(h(0) - h(-L_1)) + M_1(h^2(0) - h^2(-L_1)) + 2R_p(h(-L_1) - h(0))] + L[K_1(h(L) - h(0)) + M_1(h^2(L) - h^2(0) + 2R_p(h(0) - h(L)))] - (20)$$

$$Q_b = qZL_2[K_1(h(L + L_2) - h(L) + M_1 X(h^2(L + L_2) - h^2(L) + 2R_p(h(L) - h(L + L_2)))] - (21)$$

Where K_1, M_1 and N_1 can be given as

$$K_1 = a_c^2 C_c (N_p - N_s) - 2b_c C_c (N_p - N_s) + N_s - \frac{R\tau_p}{a} + \Phi_0 \tau_n \exp(-\alpha R_p) - (22)$$

$$M_1 = 2a b c (N_p - N_s)(\sigma\sqrt{2})^{-2} - (23)$$

$$N_1 = \frac{\Phi_0 \tau_n \exp(-\alpha R_p)}{\alpha\sigma\sqrt{2}} - a c (N_p - N_s) - (24)$$

Now, using Q (Eq.(19)) in Eq.(16) the expression for the

gate-source capacitances C_{gs} in the linear region of operation can be given by

Where P_1 is the value of P with A' and B' calculated using

$$x_1 = 0, x_2 = -L_1. \text{ Where } P$$

$$P = qZ\sigma\sqrt{2} \left[\frac{A'}{\sigma\sqrt{2}} (K_1 - M_1 R_p (\sigma\sqrt{2})^2) + M_1 B' \right] - (26)$$

Similarly the values of P_2 and P_3 are values of P with A' and B' calculated using $x_1 = L + L_2, x_2 = L$ respectively A' and B' are

$$A' = \left(\frac{qN_s}{\epsilon_s} \right)^{-1} \left[\frac{\sinh[k(h-x)]}{\sinh(k_1 L)} + \frac{\sinh(K_1 x)}{\sinh(K_1 L)} - \frac{A''}{A'''} \right] x_1 - (27)$$

A'', A''' are

$$A'' = \left[-\frac{2qN_s}{\epsilon_s K_1} \left(\frac{\sinh[k_1(L-x)]}{\sinh(K_1 L)} + \frac{\sinh(K_1 x)}{\sinh(K_1 L)} \right) - \frac{4qN_s}{\epsilon_s} \right] x_2 - (28)$$

$$A''' = \left[((D_1 + D_2 - 2R_p)^2 - \frac{2qN_s}{\epsilon_s K_1} X \right.$$

$$\left. \left(\frac{\sinh[K_1(L-x)]}{\sinh(K_1 L)} + \frac{\sinh(K_1 x)}{\sinh(K_1 L)} \right) \right] V_{gs}$$

$$B' = \frac{A' (D_1 + D_2 - 2R_p) - A'' A'''}{2 \left(\frac{qN_s}{\epsilon_s} \right)^2} - (30)$$

Similarly, the gate-drain capacitance (C_{gd}) under the linear region of operation of the optically controlled GaAs MESFET can be obtained using equation (18) in equation(16) as

$$C_{gd} = P_4 L_1 + P_5 L + P_6 L_2 - (31)$$

Where P_4 is the value of P with A^1 and B^1 calculated using $x_1 = 0, x_2 = -L_1$

Similarly, P_5 and P_6 are the values of P with A^1 and B^1 calculated using $x_1 = L, x_2 = 0$ and

$x_1 = L + L_2, x_2 = L$ respectively. And A^1 and B^1 are

$$A_1' = \left(\frac{qN_s}{\epsilon_s}\right)^{-1} \left[-\frac{\sinh[k(h-x)]}{\sinh(k_1 L)} - \frac{\sinh(K_1 x)}{\sinh(K_1 L)} - \frac{A_1''}{2A_1'} \right]_{x_2}^{x_1} \quad (32)$$

$$A_1'' = \left[\frac{2qN_s}{\epsilon_s K_n} \left(\frac{\sinh[k_1(L-x)]}{\sinh(K_1 L)} + \frac{\sinh(K_1 x)}{\sinh(K_1 L)} \right) + 2(D_1 + D_2 - 2R_p) \left(\frac{\sinh[k_1(L-x)]}{\sinh(K_1 L)} + \frac{\sinh(K_1 x)}{\sinh(K_1 L)} \right) + \frac{4qN_s}{\epsilon_s} \right]_{x_2}^{x_1} \quad (33)$$

$$A_1''' = \left[\left((D_1 + D_2 - 2R_p)^2 + \frac{2qN_s}{\epsilon_s K_n} X \left(\frac{\sinh[K_1(L-x)]}{\sinh(K_1 L)} + \frac{\sinh(K_1 x)}{\sinh(K_1 L)} \right) V_{gs} + \frac{2qN}{\epsilon_s} X(\phi_{ch}(x) + D - (V_{bi} - V_{gs} - V_{op} + V_{ds}))^{1/2} \right) \right]_{x_2}^{x_1} \quad (34)$$

$$B_1' = \frac{A_1' (D_1 + D_2 - 2R_p) - A_1''}{2\left(\frac{qN_s}{\epsilon_s}\right)^2} \quad (35)$$

In saturation region the total charge in the depletion region can be obtained using similar methodology of linear region and can be used as

$$Q_t = Q_c + Q_d + Q_e \quad (36)$$

Where Q_c , Q_d and Q_e are

$$Q_c = qZ \left[L_4 \left[K_1 (h(0) - h(-L_4)) + M_1 X (h^2(0) - h^2(-L_4) + 2R_p (h(-L_4) - h(0))) \right] + L_3 \left[K_1 (h(L_3) - h(0)) + M_1 (h^2(L_3) - h^2(0) + 2R_p (h(0) - h(L_3))) \right] \right] \quad (37)$$

$$Q_d = qZL_s \left[k_1 (h(L_3 + L_s) - h(L_3)) + M_1 (h^2(L_3 + L_s) - h^2(L_3)) + 2R_p (h(L_3) - h(L_3 + L_s)) \right] + qZL_{ex} \left[K_1 (h(L_3 + L_s + L_{ex}) - h(L_3 + L_s)) + M_1 (h^2(L_3 + L_s + L_{ex}) - h^2(L_3 + L_s)) + 2R_p (h(L_3 + L_s) - h(L_3 + L_s + L_{ex})) \right] \quad (38)$$

$$Q_e = qZL_5 \left[K_1 (h(L_3 + L_{ex} + L_5) - h(L_3 + L_{ex} + L_5)) + M_1 (h^2(L_3 + L_s + L_{ex} + L_5) - h^2(L_3 + L_s + L_{ex})) + 2R_p X (h(L_3 + L_s + L_{ex}) - h(L_3 + L_s + L_{ex} + L_5)) \right] \quad (39)$$

Now, the gate-Source capacitance in saturation of the OPFET can be evaluated using equation (36) in equation.(15) and can be given as

$$C_{gs-sat} = P_7 L_4 + P_8 L_3 + P_9 L_s + P_{10} L_{ex} + P_{11} L_5 \quad (40)$$

Where P_7 is the value of P with A' and B' calculated using

the $x_1 = 0, x_2 = -L_1$ similarly P_8, P_9, P_{10} and P_{11} are the values of P with A' and B' values calculated using

$$x_1 = 0, x_2 = -L_4, x_1 = L_3, x_2 = 0,$$

$$x_1 = L_3 + L_s, x_2 = L_3,$$

$$x_1 = L_3 + L_s + L_{ex}, x_2 = L_3 + L_s \text{ and}$$

$$x_1 = L_3 + L_s + L_{ex} + L_5, x_2 = L_1 + L_s + L_{ex}$$

Respectively A' and B' are same as given in equation(27)to

equation(30) with $V_{ds} \rightarrow V_{sat}$ similarly the gate-drain

capacitance (C_{gd-sat}) under the saturation region of

operation of the optically controlled GaAs MESFET can be modeled using equation(36) in equation(17) and can be written as

$$C_{gd-sat} = P_{12}L_4 + P_{13}L_3 + P_{14}L_s + P_{15}L_{ex} + P_{16}L_5 \quad (41)$$

Where P_{12} is the value of P with A^1 and B^1 calculated

using $x_1 = 0, x_2 = -L_1$ similarly P_{13}, P_{14}, P_{15} and

P_{16} are the values of P with A^1 and B^1 calculated using

$$x_1 = 0, x_2 = -L_4, x_1 = L_3, x_2 = 0,$$

$$x_1 = L_3 + L_s, x_2 = L_3,$$

$$x_1 = L_3 + L_s + L_{ex}, x_2 = L_3 + L_s,$$

$$x_1 = L_3 + L_s + L_{ex} + L_5, x_2 = L_1 + L_s + L_{ex}$$

respectively A^1 and B^1 are same as given in equation (32) –equation(35). With $V_{ds} \rightarrow V_{sat}$.

IV. RESULTS AND DISCUSSION

To demonstrate the validity of the proposed model the theoretical results obtained for the internal gate-source and gate-drain capacitances of the GaAs OPFETs under dark and illuminated conditions have been obtained by MATLAB. The values of parameters used for computation of model

results are $R_p = 0.1 \mu m$, $V_{bi} = 1V$, $L = 0.3 \mu m$,

$a = 0.25 \mu m$, $T_m = 0.9$, $\sigma_p = 0.02 \mu m$,

$\alpha = 10^6 / m$, $\lambda = 870nm$ and

$N_p = 4 \times 10^{23} m^{-3}$, $N_s = 1 \times 10^{21} m^{-3}$.

Variation of the internal gate-source capacitance C_{gs} and

internal gate-drain capacitance C_{gd} with V_{gs} for linear

region of operation under dark and illuminated condition is shown in Fig. 2 and Fig. 3. It is seen that both the capacitances increased with increasing incident illumination for a fixed gate-source voltage. This may be accounted by the fact that the depletion region width reduces under the illuminated condition

Figure 4 and 5 shows the gate-source capacitance

C_{gs-sat} and gate drain capacitance C_{gd-sat} in the saturation region.

It has been found that C_{gs-sat} and C_{gd-sat}

increases under illuminated condition. This may be due to the reduction in depletion width due to the photo voltage developed across the Schottky metal gate.

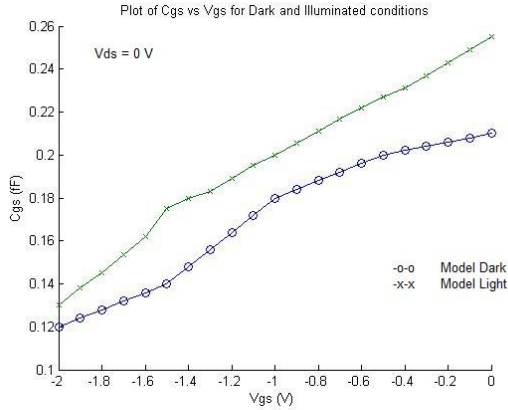


Fig.2. Plot of C_{gs} VS V_{gs} GaAs MESFET operated in linear region for dark and illuminated conditions

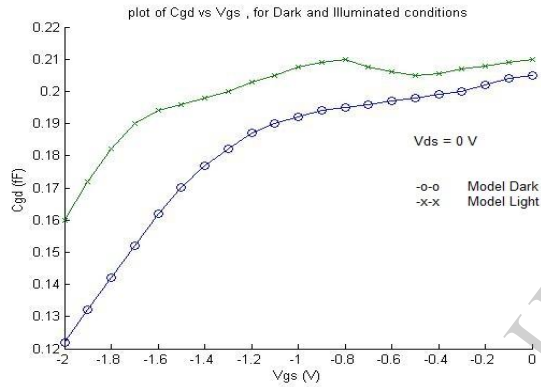


Fig.3. Plot of C_{gd} VS V_{gs} GaAs MESFET operated in linear region for dark and illuminated conditions

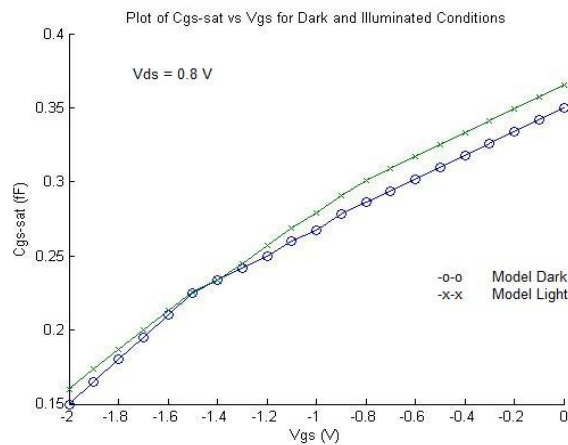


Fig.4. Plot of C_{gs-sat} VS V_{gs} GaAs MESFET operated in saturation region for dark and illuminated conditions

It can also be observed that C_{gs-sat} increases with the

increase in V_{gs} because depletion region width decreases

with the increase in gate bias (i.e. more positive V_{gs}).

From Fig.5 It can also be observed that C_{gd-sat} decreases

with the increase in V_{gs} like the conventional long channel device [23].

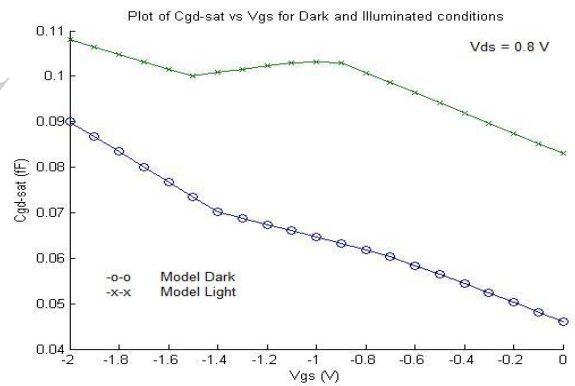


Fig.5. Plot of C_{gd-sat} VS V_{gs} GaAs MESFET operated in saturation region for dark and illuminated conditions

In Figure .6 gate-source capacitance has been plotted as a function of drain-source voltage V_{ds} . It can be seen that

gate-source capacitance becomes larger for illuminated condition. It can also be observed that gate-source capacitance decreases with the increase in V_{ds} in the linear

region and becomes nearly constant in the saturation region. Figure .7 shows the variation of gate -drain capacitance against the drain-source voltage V_{ds} . Gate-drain

capacitance increases with the increase in V_{ds} in the linear region and becomes nearly constant in the saturation region. Similar to the gate-source capacitance gate-drain capacitance is more under illuminated condition.

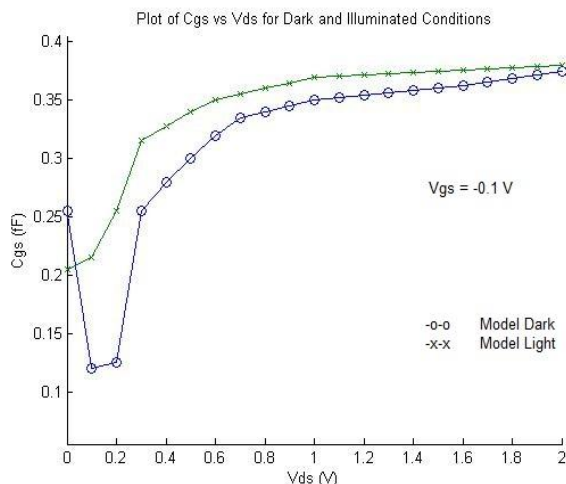


Fig.6: Plot of gate-source capacitance vs. V_{ds} of GaAs MESFET under dark and illuminated conditions

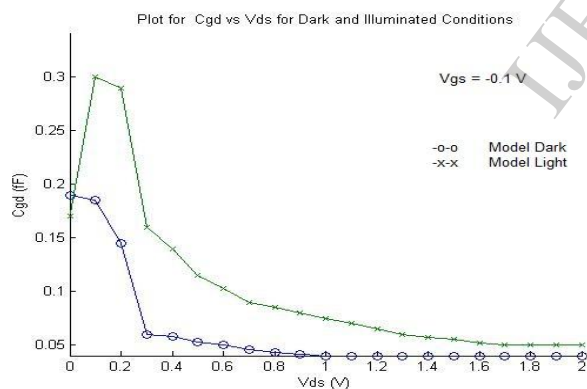


Fig. 7: Plot of gate-drain capacitance vs. V_{ds} of GaAs MESFET under dark and illuminated conditions

IV. CONCLUSION

A model for internal capacitances of GaAs MESFET has been developed. The charge for each part of the depletion region has been derived analytically for linear and saturation regions, and above results are obtained using MATLAB. The developed model may be suitably implemented for the design of photo-detectors.

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