

Kinetics Modelling of Biosorption of Bromothymol Blue onto *Gliricidia Sepium* and *Acacia* POD Composite

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Abstract:- This study reports the removal of bromothymol blue from wastewater onto *Gliricidia sepium* (*G. sepium*) and *Acacia pod* (*A. pods*) composite. The developed biocomposite mixed ratio was varied from 5 to 95 percentage composition and the effective mixture was evaluated based on methylene blue number (MBN) test. Adsorption Capacity (QE) and Removal Efficiency (RE) of the seven (7) experimental runs were studied. Cubic and quartic model were developed for RE and QE response respectively. The surface characteristics of the biosorbent was chemically modified. Fourier Transform Infrared (FTIR) was studied. Batch adsorption was investigated and effect of temperature, and biosorbent dosage were studied at various contact time and at initial concentration of 10 mg/l. Suitable kinetics model (Pseudo-first-order, Pseudo-second-order and Elovich) were studied. Cubic and Quartic model was developed for RE & QE response respectively. The RE (%) and QE (mg/g) have the highest values (96.9736 and 0.969736) at Run 3 (0.95 *G. sepium*: 0.05 *A. pods*) with lowest values at Run 2 (0.05 *G. sepium*: 0.95 *A. pods*). There was appearance and disappearance of the O-H stretch, C=O, C-F, $c \equiv c$, $\equiv C-H$ stretch groups in the unmodified and modified *G. sepium* pod at different peaks, while appearance and disappearance of C-Cl stretch, C=O, N-H bend and O-H stretch groups were noticed in the modified and unmodified *A. pod*. The result follows kinetic of pseudo-second-order and Elovich-rate models. It was observed that *G. sepium* and *A. pods* composite are effective precursors for the development of composite adsorbent due to its high yield, good QE & RE and increase in rate of adsorption.

Key words: Biosorption, Wastewater, *Gliricidia sepium*, *Acacia pods*, Kinetics, Bromothymol blue,

1. INTRODUCTION

Over the years, quality of water has been deteriorating rapidly due to the anthropogenic activities, population growth, unplanned urbanization, rapid industrialization and unskilled utilization of natural water resources. Furthermore, the increased awareness of the importance of providing impacts due to the current environmental strategies has pushed the research community towards the development of robust, economically feasible and environmentally friendly processes capable of removing pollutants from water and at same time to safeguard the health of affected populations (Sabino, Giusy, Mariangela, & Michele, 2016).

Today's highly industrialized environment is charged with a plethora of potentially toxic chemicals. The presence of harmful pollutants in the discharged wastewaters often contaminates the surface water and soil. Pollution of aquatic habitats and soil is a worldwide problem that can result in uptake and accumulation of toxic chemicals in food chains and are also harmful to the flora and fauna of affected habitats. Contamination of soil occurs when chemicals are deliberately released, by spill or underground leakage. Pesticides also play a vital role in environmental pollution. The persistent use of synthetic pesticides in agriculture, silviculture and even animal husbandry has created several difficulties on public health (Zamani, Sendi, & Ghadamyari, 2011). Problems associated with the hazards to man and environment are not confined to the developing countries, but extended to developed nations as well. The contamination of soils and groundwater with petroleum compounds is among the most prevalent problems worldwide (Alquati, Papacchini, Riccardi, Spicaglia, & Bestetti, 2005).

Industrial developments in recent years have left their impression on the environmental society (Mohamed, 2013). Many industries like the textile industry used dyes to colour their products and thus produce wastewater containing organics with a strong colour, where in the dyeing processes the percentage of dye lost waste water is 50% of the dye because of the low levels of dye-fibre fixation. Discharge of these dyes into effluents affects the people who may use these effluents for living purposes such as washing, bathing and drinking. Textile industries are one of the most common and essential sectors in the world. On the other hand, high volume of water consumption and varying wastewater characteristics due to many products, such as dyes, biocides, carriers, detergents, etc. used in the process are the factors that have caused a continuous effort to find appropriate technologies to treat textile industry wastewater (Eremektar, Selcuk, & Meric, 2007).

Recently, Low-cost by-products from agricultural, household and industrial sectors have been recognized as a sustainable solution for waste water treatment. They allow achieving the removal of pollutants from wastewater and at same time to contribute to the waste minimization, recovery and reuse. Despite numerous reviews published in the last few years, a direct comparison of

data obtained using different sorbents is difficult nowadays because of inconsistencies in the data presentation (Sameera, Naga, Srinu, & Ravi, 2011). However, there is minuscule information on kinetic study on wastewater treatment using low-cost materials. The aim of this research is to study the kinetics of less expensive adsorbents for the elimination of dyes from wastewater. Agricultural waste biocomposite *Gliricidia sepium* and *Acacia pods* will be used as adsorbents for the elimination of bromothymol blue from wastewater.

2. MATERIALS AND METHODS

2.1 Materials

The materials, *Gliricidia sepium* and *Acacia pods* were procured within the vicinity of Ladoke Akintola University of Technology (LAUTECH), Ogbomoso, Oyo state, Nigeria. They were washed with detergent and distilled water in order to completely kill the microbes present, afterwards sun-dried to constant mass (Alade et al., 2012). They were subsequently blended into smaller and uniform particle size using a blender and sieve analyzer respectively. The grinded *G. sepium* and *A. pods* were subsequently modified using hydrogen peroxide continuously until a clear solution was achieved. It was then oven dried till constant mass and kept safely for further use.

2.2 Adsorption of Methylene blue

Adsorption of Methylene-blue dye was carried out according to the procedures described by (Alade et al., 2012), with slight modifications. Grinded and decolorized biocomposite of *G. sepium* and *A. pods* (1 g, 0.95:0.05) soaked in 100 ml methylene blue dye (10 mg/L), then left for 24 hours. The solution was decanted and taken for UV analysis using a spectrophotometer to determine the un-adsorbed dye concentrations.

2.3 Design of Experiment

The design of the experiment is generally undertaken to minimize time, materials and invariably cost, involve in experimental design. Design-Expert software (Version 11.0.4.0). The experimental design information is expressed in Table 1 below.

Table 1. Experimental design information

Study Type	Mixture
Design Type	Simplex Lattice
Design Model	Cubic
Build Time (ms)	2.00
Subtype	Randomized
Runs	7
Blocks	No Blocks

The independent variables were adsorption temperature (room temperature), dosage (1 g), concentration (10mg/L), and time (24 hrs), giving two response variables, response 1 is the adsorption capacity” while response 2.00 is the “removal efficiency”. The experimental values are expressed in Table 2 below.

Table 2. Response derivatives

Response Name	Units	Observations	Analysis	Transform	Model
R1	Adq mg/g	5	Polynomial	Power	Cubic
R2	RE %	6	Polynomial	Power	Quartic

Table 3. Component Mixture

Component	Unit	Level	
		low	High
<i>Gliricidia sepium</i>	%	5	95
<i>Acacia pod</i>	%	5	95

Table 4. Experimental design of biocomposite mix used

Run	Gliricidia (%)	sepium (%)	Acacia (%)	Absorbance (abs)	Adsorption capacity (QE) mg/g	Removal efficiency (RE) (%)
1	65		35			
2	5		95			
3	95		5			
4	35		65			
5	72.5		27.5			
6	50		50			
7	27.5		72.5			

2.4 Fourier Transmission Infrared Spectroscopy Analysis

The spectrum is a graph which contains percent transmittance along Y axis and frequency or wavelength along X axis. By studying the peak between a particular frequency i.e. gap or band, type of the functional group present was predicted. For the case of Mango seed kernel and Papaya seeds, FTIR shows the change in properties of the surface of biosorbent on addition of RR dye (Tariku, 2016).

2.5 Batch Adsorption of Bromothymol Blue from wastewater using *Gliricidia sepium* and *Acacia seed pod* Biosorbent

Certain quantity of the stock solution was taken to conduct batch experiments for dye adsorption. The parameter of the factors that affect the adsorption process (adsorbent dosage, concentration of adsorbate, temperature and contact time will be studied). For this experiment, the process of adsorption of bromothymol blue on *G. sepium* and *Acacia seed pod* were studied (Bhanuprakash & Belagali, 2017). A known amount of this solution will be taken in different numbers of beakers for different masses of the adsorbent and thereafter, adsorption will be studied with different concentrations of the bromothymol blue (Bhanuprakash & Belagali, 2017).

The percentage removal of the dye by each adsorbent was calculated from the relation:

$$Re = \frac{C_o - C_e}{C_o} \times 100\% \quad (2.1)$$

Where C_o and C_e are the concentrations (mg/L) of the dye initially and at equilibrium time (Bhattacharya, Naiya, Mandal, & Das, 2008).

The adsorbed amount q_e was calculated from the relation:

$$q_e = \frac{(C_o - C_e)V}{w} \quad (2.2)$$

2.6 Effect of Varying Factors

Temperature and biosorbent dosage were varied on the adsorption rate and removal efficiency at initial concentration of 10 mg/l across various contact time.

2.6.1 Effect of Biosorbent Dosage

The effect of biosorbent dose on the adsorption of 10 mg/l of Bromothymol blue is studied across dose 1g, 1.5 g and 2 g.

2.6.2 Effect of Temperature

The effect of temperature on the adsorption of 10 mg/l of Bromothymol blue is studied across temperature 40°, 50° and 60° Celsius.

2.7 Adsorption kinetics

Contact time from experimental results can be used to study the rate-limiting step in the adsorption process in terms of the kinetic energy. The overall adsorption process can be controlled either by one or more steps such as pore diffusion, surface diffusion or a combination of more than one step. Lagergen's first order equation and Ho's second order equation are such examples of kinetic models commonly used to describe these adsorption kinetic models (Ho, 2006).

2.7.1 The pseudo first-order kinetic

The pseudo first order kinetic equation of Lagergren model is given as such equations (Lagergren, 2009). Pseudo first order equation refers to the assumption of the rate of change of solute uptake with time, which is directly proportional to the difference in the saturation concentration and the amount of solid uptake with time (Khaled, *et al* 2009).

$$\frac{d_q}{d_t} = K_1 (q_e - q_t) \quad (2.3)$$

where q_e and q_t are the amount of adsorbed waste (mg/g) at an equilibrium and at any instant of time t (min), respectively and k_1 is the rate constant of pseudo first order adsorption operation (min).

2.7.2 The Pseudo second order Kinetic

The pseudo second order kinetic equation is given as (Ho, 1995):

$$\frac{d_q}{d_t} = k(q_e - q_t)^2 \quad (2.4)$$

The pseudo second order model is based on the assumption that the rate-limiting step may stem from the chemical adsorption involving valence forces through the sharing or exchange of electrons between the adsorbent and adsorbate (Ho & McKay, 1999).

The linearize equation for pseudo second order is written as

$$\frac{t}{qt} = \frac{1}{k_2 q_e^2} + \frac{t}{q_e} \quad (2.5)$$

A plot of $\frac{t}{qt}$ against t gives a straight line with a slope of $1/q_e$ and an intercept of $\frac{1}{k_2 q_e^2}$

2.7.3 The Elovich Model

The equation defining the Elovich model is based on a kinetic principle assuming that the adsorption sites increases exponentially with adsorption, which implies a multilayer adsorption. It is expressed by the relation:

$$\frac{qe}{qm} = K_E C_e \exp\left(-\frac{qe}{qm}\right) \quad (2.6)$$

The linearize equation for the Elovich model is written as;

$$\ln \frac{qe}{c_e} = \ln K_E q_m - \frac{qe}{qm} \quad (2.7)$$

A plot of $\ln \frac{qe}{c_e}$ against qe gives a straight line with a slope of $-1/q_m$ and an intercept of $\ln \frac{qe}{c_e}$

3. RESULTS AND DISCUSSION

3.1 Adsorption capacity and Removal Efficiency of Methylene Blue onto the Biocomposite

The experimental design with seven (7) runs for which data was provided in Table 2.4 for adsorption capacity (mg/g) and removal efficiency (%) gives the following results expressed in Table 5 & 6 below for which mixture loading is L-Pseudo, with transformation power of lambda, λ raised to the power of -3 having no constant. Suitable models for adsorption capacity and removal efficiency were usually selected based on the highest order polynomials.

The Quartic model has the highest R^2 value (0.9999) and lowest standard deviation (0.0010) for the adsorption capacity while in Removal efficiency the Cubic model has the highest R^2 value (1.0000) and lowest standard deviation (0.0096) and expressed in the model summary statistics, table 5 & 6 below was selected accordingly for this study. The suitability of the model was further supported with the least value (0.0138) of the Predicted Residual Error Sum of Squares (PRESS) for the adsorption capacity, while that of removal efficiency has a PRESS value of 0.0347. The positive and negative coefficients indicated positive and negative influences of the independent variables on the selected responses.

Table 5. Model Summary Statistics for Adq

Source	Sequential p-value	Adjusted R ²	Predicted R ²	Std. Dev.	R ²	PRESS
Linear	0.1960	0.2192	-1.4079	0.0341	0.3753	0.0180
Quadratic	0.1269	0.5778	-0.8613	0.0251	0.7467	0.0139
Cubic	0.6361	0.4506	-72.4908	0.0286	0.7802	0.5479
Quartic*	0.0162	0.9993	-0.8570	0.0010	0.9999	0.0138

*Suggested Results are means of duplicate values.

Table 6. Model Summary Statistics for RE

Source	Sequential p-value	Adjusted R ²	Std. Dev.	R ²	PRESS
Linear		0.0941	0.5486	0.5119	3.60
Quadratic		0.0741	0.9034	0.2368	3.09
Cubic*		0.0182	0.9998	0.0096	0.0347

*Suggested Results are means of duplicate

3.1.1 ANOVA of Adsorption capacity (Cubic model) and Removal Efficiency (Quartic model)

The analysis of variance (ANOVA) procedure was used to determine the significance of variables and to substantiate the adequacy of the quadratic regression model obtained in this study. The significance of the model was based on the principle of the Fisher's statistical test (F-test) and it generates the F-value, which represents the ratio of the mean square of regression to the mean error. Significance of the model terms were further tested based on lower probability (p-value) which may lie between 90 % confidence level (Hegazi, 2012). Lack of fit, which is usually preferred to be insignificant, was also used as diagnostic test to determine the adequacy of any model developed (Halder 2015). The results of the ANOVA are presented in Table 7.

Mixture Component coding is L_Pseudo for adsorption capacity and removal efficiency. Sum of squares is Type III – Partial. The Model F-value for adsorption capacity and removal efficiency are 1766.28 and 8446.28, respectively. These values imply there are 1.78% and 0.80% chances that an F-value this large could occur due to noise. P-values less than 0.0500 indicate model terms are significant.

Table 7. ANOVA for Response Surface model Analysis for adsorption capacity

Source	Adsorption Capacity				Removal Efficiency			
	Sum of Squares	Mean Square	F-value	p-value	Sum of Squares	Mean Square	F-value	p-value
Model	0.0075	0.0019	1766.28	0.0178	2.32	0.7741	8446.28	0.0080
^(a) Linear Mixture	0.0028	0.0028	2652.12	0.0124	1.54	1.54	16761.38	0.0049
AB	0.0006	0.0006	596.44	0.0261	0.6438	0.6438	7024.29	0.0076
AB(A-B)	0.0011	0.0011	1025.40	0.0199	0.1121	0.1121	1222.61	0.0182
Residual	1.055E-06	1.055E-06			0.0001	0.0001		
Cor Total	0.0075				2.32			

P > 0.10

3.1.2 Fit Statistics for Adsorption capacity and removal efficiency

The adsorption capacity negative **Predicted R²** of -0.8570 implies that the overall mean may be a better predictor of your response than the current model. In some cases, a higher order model may also predict better. While for removal efficiency, a positive **Predicted R²** 0.9851 is close to the **Adjusted R²** of 0.9998 which is what one normally expect; i.e. the difference is not greater than 0.2. It may indicate a large block effect or a possible problem with your model and/or data if the difference is greater than 2. Things to consider are model reduction, response transformation, outliers, etc. All empirical models should be tested by doing confirmation runs.

Adeq Precision measures the signal to noise ratio. A ratio greater than 4 is desirable. The ratio of adsorption capacity and removal efficiency are 129.454 and 210.834 respectively, these values indicate an adequate signal. These model can be used to navigate the design space. Table viii gives indication of the lower and upper limits for the adsorption capacity and removal efficiency, it also expresses lower and upper weights which are the same for both adsorption capacity and removal efficiency.

3.1.3 Constraints and Solutions

The constraint of the biocomposite mix ratio are presented in Table 9. The plots are expressed in fig. 3.1, 3.2, 3.3 and 3.4, constituting the mix ratio making up the biocomposite for both RE and QE.

Table 8. Statistics for adsorption capacity

Properties	Adsorption Capacity	Removal Efficiency
	Values	Values
Std. Dev.	0.0010	0.0096
Mean	1.16	95.62
C.V. %	0.0887	0.0100
R ²	0.9999	1.0000
Adjusted R ²	0.9993	0.9998
Predicted R ²	-0.8570	0.9851
Adeq Precision	129.4540	210.8337

Table 9. Required constraints showing the limit of the response

Name	Goal	Lower Limit	Upper Limit	Lower Weight	Upper Weight	Importance
A:A	is in range	5	95	1	1	3
B:B	is in range	5	95	1	1	3
Adq	Minimize	1.09658	1.21784	1	1	3
RE	Minimize	95.1679	96.9736	1	1	3

Table 10. Solutions

Number	A	B	Adq	RE	Desirability
1	5.000	95.000	0.970	96.974	1.000
2	93.253	6.747	0.944	95.197	0.062
3	95.000	5.000	0.952	95.169	0.015

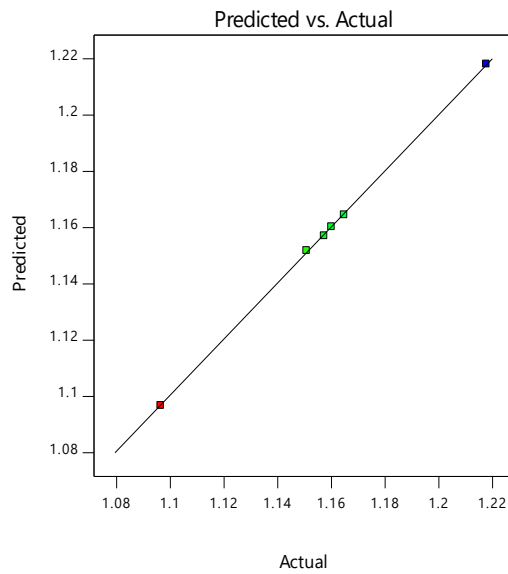


Fig. 3.1 Plot of Predicted versus Actual values for adsorption capacity

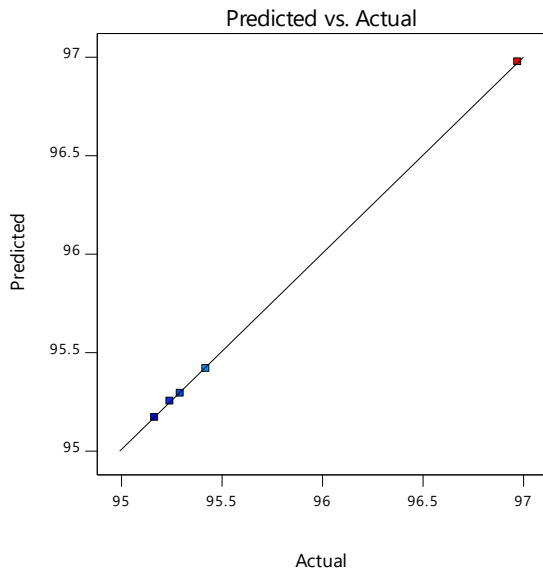
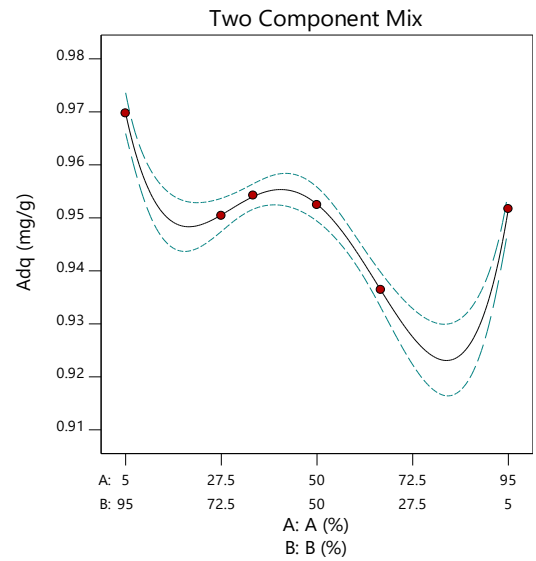
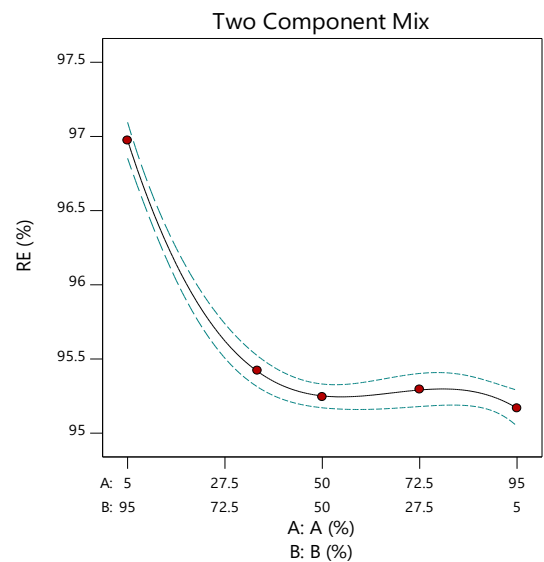


Fig. 3.2 Plot of Predicted versus Actual values for removal efficiency



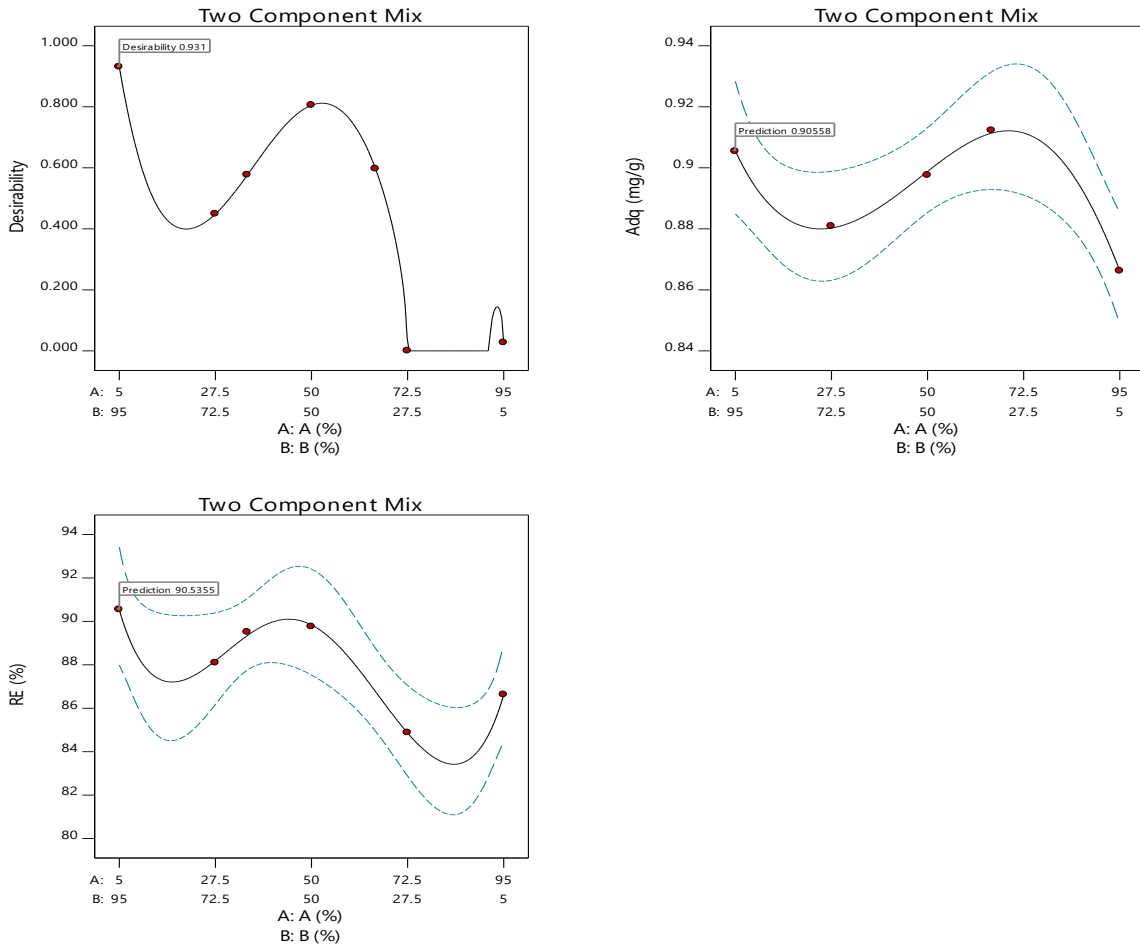


Fig. 3.3 Plots of RE, Adq and desirability

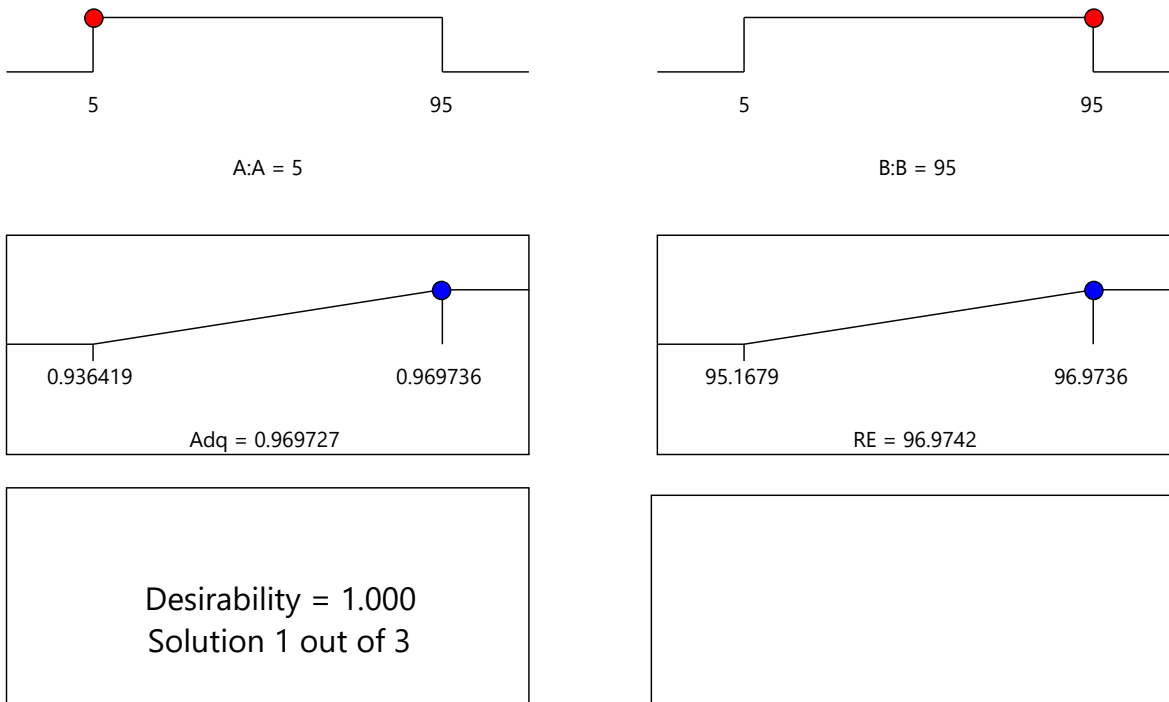


Fig. 3.4 Responses of the RE, Adq and desirability plots

3.2 Fourier Transform Infrared Spectroscopy (FTIR)

The presence of various functional groups presents on the surface of the adsorbent and their role in adsorption was analyzed using FTIR (Fourier transform infrared) spectrum within the range of 400–4000 cm^{-1} using Thermo-Fisher FT-IR analyzer (SCIENTIFIC, NICOLET 5700). The presence of these functional group in the activated carbon will be responsible for adsorption for different heavy metal from aqueous solution (Rai *et al.*, 2015). The FTIR spectra of *G. sepium* unmodified, *G. sepium* modified, Acacia unmodified and Acacia modified are represented in Table 11 and 12 respectively. The IR peak observed in the *G. sepium* unmodified ranges from 612.2 to 3957.6 while the modified ranges from 609.5 to 3964.2. It was observed from table xi that the peak height for the unmodified *G. sepium* ranges from 5.0 to 16.1 while the peak height for the modified ranges from 1.9 to 8.1.

In Acacia pod, it was observed that the unmodified IR peak ranges from 636.6 to 3964.2 while the IR peak for the modified ranges from 610.2 to 3964.1. The peak height for the unmodified and the modified ranges from 2.9 to 14.0 and 0 to 9.0 respectively. Some changes were observed in the functional groups of both samples and these were presented in table 11 and 12. There was the appearance of the C= stretch at peak of 5.7 cm^{-1} and O-H stretch at peak of 5.7 cm^{-1} after the modification of *G. sepium*. It was also observed that in Acacia there was an appearance of the N-H stretch at peak height of 4.1 cm^{-1} and C-O stretch at a peak height of 5.9 cm^{-1} . The FTIR helps to reveal whether a reduction, appearance, disappearance or broadening of the peaks after the modification with hydrogen peroxide has occurred by the spectrum of the sample (Olajire, Abidemi, Lateef, & Benson, 2017).

Table 11. FTIR Spectra changes and peak height for *Gliricidia sepium*

Untreated <i>G. sepium</i>			Treated <i>G. sepium</i>			
Peak	Bond Type	Peak height	Peak	Bond Type	Peak height	Remark
612.2	C-Br stretch	8.4	609.5	C-Br stretch	4.4	Shifted downward
726.3	=C-H bend	10.2	737.1	C-H bend	4.3	Shifted upward
775.3	C-Cl stretch	10.1	787.0	C-Cl stretch	5.6	Shifted upward
874.5		11.4	874.3		5.1	
989.2	=C-H bend	11.1	949.8	=C-H bend	4.6	Shifted downward
1023.1	C-F stretch	8.6	1013.7	C-F stretch	3.9	Shifted downward
1076.8	C-F stretch	6.1	1059.8	C-F stretch	3.0	Shifted downward
1155.0	C=O stretch	6.2	1119.8	C-O stretch	3.4	Shifted downward
1208.6	C=O stretch	11.3				Disappear
			1240.5	C-O stretch	4.9	Appear
1281.0	C-F stretch	11.2	1272.8	=C-F stretch	4.2	Shifted downward
			1359.8	C-F stretch	6.3	Appear
1469.3	C-H bend	10.6	1444.9	C-H bend	4.8	Shifted downward
			1494.1	C=C stretch	5.7	Appear
1544.0	N-H bend	9.6	1552.0	N-H bend	4.5	Shifted upward
1639.2	C=O stretch	8.1	1677.6	C=O stretch	4.2	Shifted upward
1709.0	C=O stretch	7.6	1732.9	C=O stretch	3.8	Shifted upward
1757.5	C=O symmetric	9.1	1794.9	C=O stretch	5.7	Shifted upward
1911.1		15.1	2016.8		6.9	
2004.7		14.2	2077.8		6.9	
2081.7		14.2				
2152.1	$C \equiv C$ stretch	16.1				Disappear
2226.4	$C \equiv C$ stretch	15.4				Disappear
			2281.4	$C \equiv C$ stretch	7.0	Appear
2300.0		15.0				
2404.0		14.1				
2443.0		14.3				
2533.1	O-H stretch	13.0	2352.0		8.1	Disappear
2585.4	O-H stretch	12.3	2482.1	O-H stretch	6.2	Shifted downward
2693.9	O-H stretch	12.3	2604.8	O-H stretch	5.4	Shifted downward
			2724.9	O-H stretch	5.7	Appear
2762.5	O-H stretch	11.3	2785.1	O-H stretch	5.5	Shifted upward
2825.8	O-H stretch	11.6	2855.2	O-H stretch	5.3	Shifted upward
2909.3	C-H stretch	9.1	2922.2	C-H stretch	4.4	Shifted upward
2957.1	C-H stretch	9.7				Disappear
3049.8	=C-H stretch	9.0	3022.6	=C-H stretch	5.0	Shifted downward
3127.4	=C-H stretch	7.5	3084.0	=C-H stretch	4.1	Shifted downward
3219.8	N-H symmetric	6.7	3162.1	N-H symmetric	3.6	Shifted downward
			3223.2	$\equiv C - H$ stretch	3.5	Appear
3327.0	O-H stretch	6.7	3306.3	O-H stretch	3.7	Shifted downward
3400.8	O-H stretch	6.3				Appear
3460.1	O-H	5.0	3451.4	O-H stretch	2.0	Shifted downward
3497.6	O-H stretch	5.7	3517.9	O-H stretch	1.9	Shifted upward
3569.6	N-H stretch	7.4	3583.7	N-H stretch	2.6	Shifted upward
3616.0	N-H stretch	6.6	3661.6	N-H stretch	3.9	Shifted upward
3700.8	N-H stretch	12.3	3725.0	N-H stretch	5.3	Shifted upward
3773.1	N-H stretch	10.6	3782.4	N-H stretch	5.4	Shifted upward
3838.4	N-H stretch	10.7	3840.3	N-H stretch	5.6	Shifted upward
3898.4	N-H stretch	10.6	3903.7	N-H stretch	4.3	Shifted upward
3957.6	N-H stretch	11.5	3964.2	N-H stretch	6.0	Shifted upward

Table 12. FTIR Spectra changes and peak height for Acacia pod

Untreated <i>Acacia</i>			Treated <i>Acacia</i>			
Peak	Bond Type	Peak height	Peak	Bond Type	Peak height	Remark
			610.2	C-Cl stretch	4.8	Appear
636.6	C-Cl stretch	7.6				Disappear
725.1	C-Br stretch	7.6	714.1	C-Br stretch	6.4	Shifted downward
788.3	C-Cl stretch	7.5	769.8	C-Cl stretch	7.3	Shifted downward
877.7	=C-H bend	8.7	875.1	=C-H bend	7.7	Shifted downward
966.7	=C-H bend	6.4	982.3	=C-H bend	2.1	Shifted upward
1074.3	C-F stretch	4.6	1073.5	C-F stretch	0.5	Shifted downward
1147.1	C-F stretch	4.9	1148.6	C-F stretch	0	Shifted upward
1243.0	C-F stretch	7.2	1233.7	C-F stretch	0.4	Shifted downward
1287.9	C-F stretch	8.6	1291.0	C-F stretch	0.6	Shifted upward
1364.0	C-F stretch	9.9	1380.2	C-F stretch	4.5	Shifted upward
1463.8	C-H bend	7.9	1470.7	C-C bend	6.2	Shifted upward
1530.2	C=H bend	8.0	1555.2	C=H bend	6.1	Shifted upward
			1655.2	C=O stretch	6.4	Appear
			1683.9	C=O stretch	6.2	Appear
1694.2	C=O stretch	3.6				Disappear
			1748.3	C=O stretch	5.9	Appear
2020.6		11.9	2004.3		8.5	
2082.4		12.3	2078.6		8.4	
2248.1	$C \equiv N$ stretch	13.6	2253.0	$C \equiv C$ stretch	8.3	Shifted upward
2342.4		14.0	2365.9		2.3	
2443.1		13.3	2432.0		8.9	
2515.2	O-H stretch	11.7	2533.8	O-H stretch	5.9	Shifted upward
2606.7	O-H stretch	11.6	2587.2	O-H stretch	9.0	Shifted downward
2717.4	O-H stretch	10.7	2691.2	O-H stretch	7.4	Shifted downward
2787.0	O-H stretch	9.8	2749.8	O-H stretch	9.0	Shifted downward
2852.5	O-H stretch	7.2	2832.7	O-H stretch	6.8	Shifted downward
2889.8	O-H stretch	8.7	2886.4	O-H stretch	4.7	Shifted downward
2938.4	O-H stretch	6.0	2963.9	O-H stretch	3.5	Shifted upward
3038.6	=C-H stretch	6.7	3051.3	=C-H stretch	5.4	Shifted upward
3101.3	O-H stretch	5.4	3101.6	O-H stretch	4.4	Shifted upward
			3141.9	O-H stretch	4.0	Appear
3200.7	O-H stretch	4.9	3203.7	O-H stretch	1.7	Shifted upward
3306.6	O-H stretch	3.0	3271.0	O-H stretch	0.4	Shifted downward
3367.1	O-H stretch	2.9	3384.9	O-H stretch	1.1	Shifted upward
3433.8	O-H stretch	4.0	3441.4	O-H stretch	1.8	Shifted downward
3485.4	O-H stretch	4.1	3501.0	O-H stretch	0.9	Shifted upward
3538.3	O-H stretch	3.4	3561.6	O-H stretch	-0.1	Shifted downward
3590.7	O-H stretch	3.5	3617.8	O-H stretch	-0.5	Shifted upward
3650.5	O-H stretch	5.4	3687.8	O-H stretch	0.1	Shifted upward
3763.2	N-H stretch	9.7	3753.5	N-H stretch	0.9	Shifted downward
3842.4	N-H stretch	9.2	3846.1	N-H stretch	2.3	Shifted upward
3884.7	N-H stretch	8.7				Disappear
3964.2	N-H stretch	9.9	3964.1	N-H stretch	4.1	Shifted upward

3.3 Effect of Biosorbent Dosage

3.3.1 QE and RE study

Effect of biosorbent dose of the adsorbent composite mix was greatly influenced in the adsorption process using *G. sepium* and *Acacia* pods. The dose of biosorbent at various time from 15 minutes to 210 minutes were investigated for biosorbent dose 1g, 1.5 g and 2 g and the results is given. It was observed from the plot of QE against time shows that the adsorption capacity increased with increasing time from 15- 210 minutes. It was also observed that the adsorption capacity decreased with increasing biosorbent dose.

It was observed that the maximum adsorption capacity for all considered dose occurred at 210 minutes and the values are estimated to be 0.819767 mg/g, 0.624031 mg/g, and 0.485465 mg/g for 1 g, 1.5 g and 2 g respectively. The lowest adsorption capacities were observed to occur at 15 minutes with the data estimated as 0.491279 mg/g, 0.554264 mg/g and 0.44186 mg/g for 1 g, 1.5 g and 2 g respectively. The trend from the adsorption capacity results from studied concentrations shows that adsorption capacity decreases with increase in biosorbent dose and it is in agreement with results in a similar study by Amuda et al., (2013).

Biosorbent dose also affects the removal efficiency during adsorption process. The removal efficiencies were observed to increase with an increase in time from 15-210 minutes also with an increase in biosorbent dose across 1 g, 1.5 g and 2 g. The maximum experimented RE for all concentrations were calculated to be 82 %, 94 % and 97 % for 1 g, 1.5 g and 2 g respectively. The lowest removal efficiency for concentration 1 g, 1.5 g and 2 g are 49%, 83% and 88 % respectively. The trend from this

results shows that increase in biosorbent dose increases the removal efficiency of the adsorbate and it is in consonance with previous study by Amuda et al., (2014).

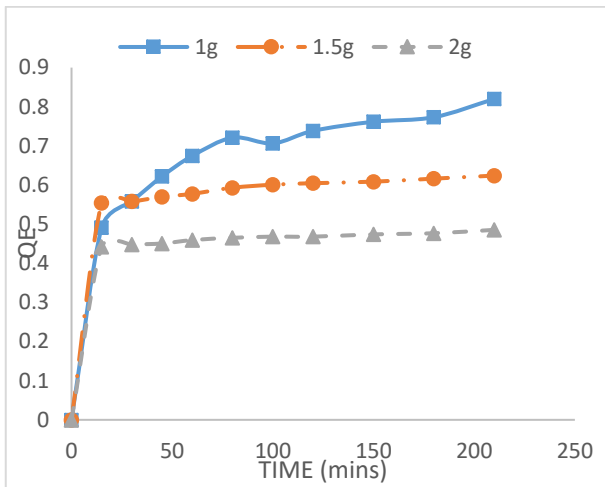


Fig. 3.5 Plot of QE against Time

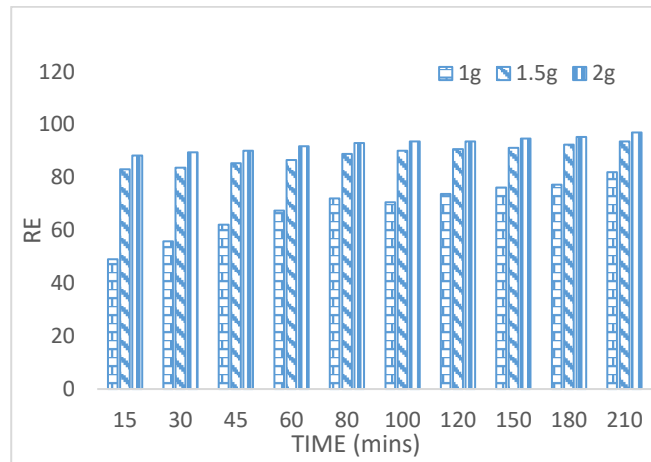


Fig. 3.6 Plot of RE against Time

3.3.2 Kinetics Study

Pseudo-First Order Kinetic models

The plot of $\ln(Q_e - Q_t)$ against time describes the relationship between the pseudo-first order kinetics constant as obtained from the slope and intercept of the plot for 1 g, 1.5 g and 2 g. The kinetic parameter for each of the concentration obtained are K_1 , q_e cal, q_e experimental and R^2 . The q_e cal parameter are estimated to be 0.3350, 0.0930 and 0.0495 for biosorbent dose 1 g, 1.5 g and 2 g respectively. The q_e experimental parameter obtained are 0.819767, 0.624031 and 0.485465 for biosorbent dose 1 g, 1.5 g and 2 g respectively. It is generally observed that there is a variation between the q_e cal and the q_e exp for all the dose; as such it indicates that pseudo-first order poorly fit the data (Skrkalj and Malina, 2011).

The K_1 values estimated are 0.0117, 0.0134, 0.0097 for biosorbent dose 1 g, 1.5 g and 2 g respectively. The estimated R^2 parameter are 0.9550, 0.9704, 0.9814 for biosorbent dose 1 g, 1.5 g and 2 g respectively. The R^2 values is less than that of Pseudo-second order (0.9968, 0.9996, 0.9996) for the three biosorbent dose and Elovich R^2 values 0.9936, 0.9866 for dose 1g and 1.5g respectively. This buttress the point that pseudo-first order model is poorly fit for the data.

Pseudo-Second Order Kinetic models

The plot of t/q against t was used to evaluate K_2 , q_e exp, q_e cal and R^2 for the pseudo-second order model equation parameters. The K_2 obtained for 1 g, 1.5 g and 2g biosorbent dose are 0.0932, 0.0782 and 0.0766 respectively. The q_e cal parameter are estimated to be 0.8540, 0.6312 and 0.4872 for biosorbent dose 1 g, 1.5 g and 2 g respectively. The q_e experimental parameter obtained are 0.819767, 0.624031 and 0.485465 for biosorbent dose 1 g, 1.5 g and 2 g respectively.

The closeness between the q_e cal and q_e exp for both concentration and this suggests that pseudo-second order fitted the adsorption data better than Pseudo-first order. The estimated R^2 parameter for the model is 0.9968, 0.9996, 0.9996 for biosorbent dose 1 g, 1.5 g and 2 g respectively. The R^2 values is well fitted compared to Pseudo-first order (0.9550, 0.9704, 0.9814) and Elovich (0.9936, 0.9866, 0.9601). High R^2 values obtained for pseudo-second order further emphasizes the suitability over pseudo-first order and Elovich model.

Elovich Kinetic models

The plot of $\ln(q_e/c_e)$ against q_e describes the relationship between the Elovich kinetics constant as obtained from the slope and intercept of the plot for 1g, 1.5 g and 2g. The kinetic parameter for each of the concentration obtained are K_E , q_m and R^2 . The q_m parameter estimated are -0.2166, -0.0664, -0.0313 for biosorbent dose 1 g, 1.5 g and 2 g respectively. The K_E were estimated to be -0.0440, -0.0116 and -8.19E-6 for biosorbent dose 1 g, 1.5 g and 2 g respectively. The correlation coefficient R^2 for the Elovich model is estimated to be 0.9936, 0.9866, 0.9601 for biosorbent dose 1 g, 1.5 g and 2 g respectively. The R^2 values are well fitted compared to the pseudo-first order kinetic model values (0.9550, 0.9730, 0.8699).

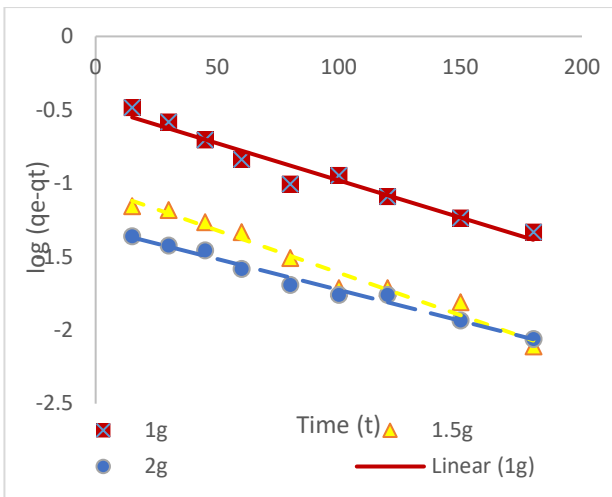


Fig. 3.7 Pseudo-first order kinetic plot of Ln (Qe - Qt) against time (mins) at different dosage

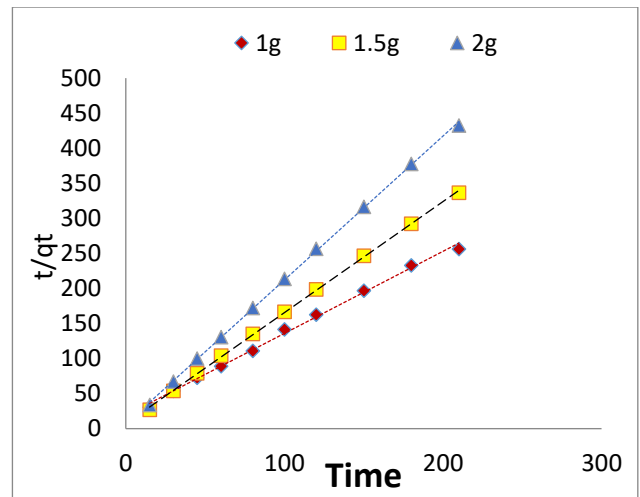


Fig. 3.8 Pseudo-second Order plot of T/Q against Time (t) at different biosorbent dose

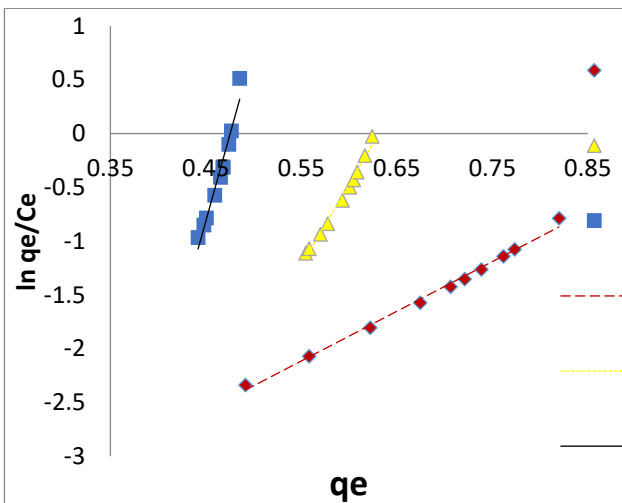


Fig. 3.9 Elovich plot of ln qe/ce against qe for effect of biosorbent dosage

3.4 Effect of Temperature

3.4.1 QE and RE study

Effect of temperature has a great influence in the adsorption process using *G. sepium* and *Acacia pods*. The effect of temperature at various time from 15 minutes to 210 minutes were investigated for temperature 40°, 50° & 60° Celsius and the results is given. It was observed from the plot of QE against time that the adsorption capacity increased with increasing time from 15- 210 minutes. It was also observed that the adsorption capacity decreases with increasing temperature from 40°-60° Celsius.

The maximum adsorption capacity for all temperatures were observed to occur at 210 minutes and the values are estimated to be 0.755814 mg/g, 0.715116 mg/g, and 0.700581 mg/g for 40°, 50° and 60° Celsius respectively. The lowest adsorption capacities were observed to occur at 15 minutes with the data estimated as 0.531977 mg/g, 0.436047 mg/g and 0.43314 mg/g for 40°, 50° and 60° Celsius respectively. The trend from the adsorption capacity results from studied concentrations shows that adsorption capacity decreases with increase in temperature and it is in agreement with results in earlier reports (Satapathy et al., 2013).

Removal efficiency has been greatly affected by temperature during adsorption process. The removal efficiencies were observed to increase with an increase in time from 15-210 minutes but decreases with an increase in temperature across 40°, 50° and 60° Celsius. The maximum experimented RE for all temperatures were calculated to be 76%, 72% and 70% for 40°, 50° and 60° Celsius respectively. The lowest removal efficiency for the temperature 40°, 50° and 60° Celsius are 53%, 44% and 43% respectively. The trend from this results shows that increase in temperature decreases the removal efficiency of the adsorbate. This phenomenon indicates that the adsorption process was exothermic in nature it is in consonance with earlier studies by (Satapathy et al. 2013; Girish and Murty 2014; Inyinbor et al. 2016 a, b).

3.4.2 Kinetics Study

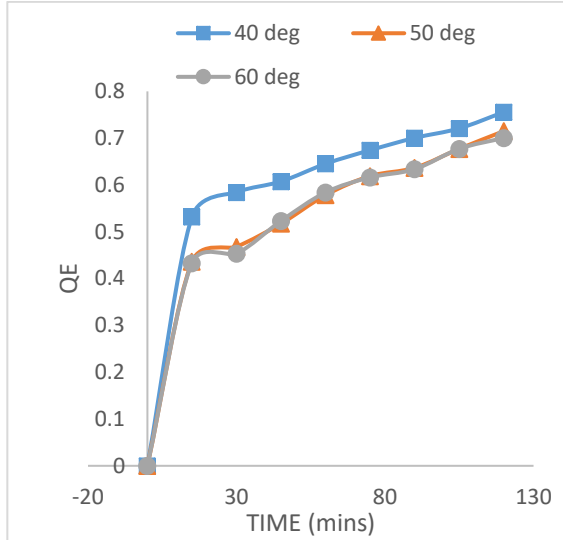


Fig. 3.10 Plot of QE against Time

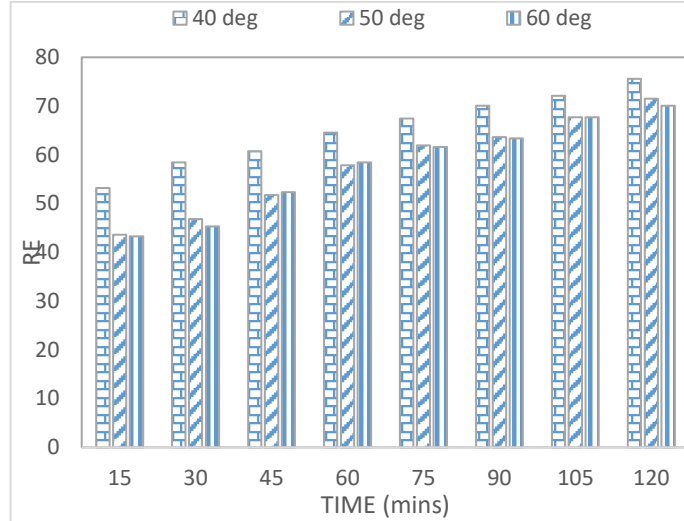


Fig. 3.11 Plot of RE against Time

Pseudo-First Order Kinetic models

The q_e cal parameter are estimated to be 0.3330, 0.4600 and 0.5000 for temperature 40°, 50° and 60° Celsius respectively. The q_e experimental parameter obtained are 0.755814, 0.715116 and 0.700581 for temperature 40°, 50° and 60° Celsius respectively.

The K_1 values estimated are 0.0200, 0.0214, 0.0253 for temperature 40°, 50° and 60° Celsius respectively. The estimated R^2 parameter are 0.9757, 0.9537, 0.9251 for temperature 40°, 50° and 60° Celsius respectively. The R^2 values is less than that of Pseudo-second order (0.9937, 0.9859, 0.9890) and Elovich (0.9980, 0.9860, 0.9994), from these values it can be deduced that it is a poorly fitted data compared to other models studied.

Pseudo-Second Order Kinetic models

The K_2 obtained for temperature 40°, 50° and 60° Celsius are 0.1039, 0.0614, 0.0639 respectively. The q_e cal parameter from table 4.20 are estimated to be 0.8041, 0.8030 and 0.7935 for temperature 40°, 50° and 60° Celsius respectively. The q_e experimental parameter obtained are 0.755814, 0.715116 and 0.700581 for temperature 40°, 50° and 60° Celsius respectively. There is closeness between the q_e cal and q_e exp for all temperature and this suggests that pseudo-second order fitted the adsorption data better than Pseudo-first order. The estimated R^2 parameter for the model is 0.9937, 0.9859, 0.9890 for temperature 40°, 50° and 60° Celsius respectively. The R^2 values is well fitted compared to Pseudo-first order (0.9757, 0.9537, 0.9251) but less of a good fit compared to Elovich (0.9980, 0.9860, 0.9994). High R^2 values obtained for pseudo-second order further emphasizes the suitability over pseudo-first order.

Elovich Kinetic models

The q_m parameter estimated are -0.2247, -0.1812, -0.2409 for temperature 40°, 50° and 60° Celsius respectively. The K_E were estimated to be -0.0465, -0.0211 and -0.0521 for temperature 40°, 50° and 60° Celsius respectively. The correlation coefficient R^2 for the Elovich model are estimated to be 0.9980, 0.9860, 0.9994 for temperature 40°, 50° and 60° Celsius respectively. The R^2 values are well fitted compared to the pseudo-first order kinetic model values (0.9757, 0.9537, 0.9251) and pseudo-second order (0.9937, 0.9859, 0.9890) and this emphasizes the suitability of the model.

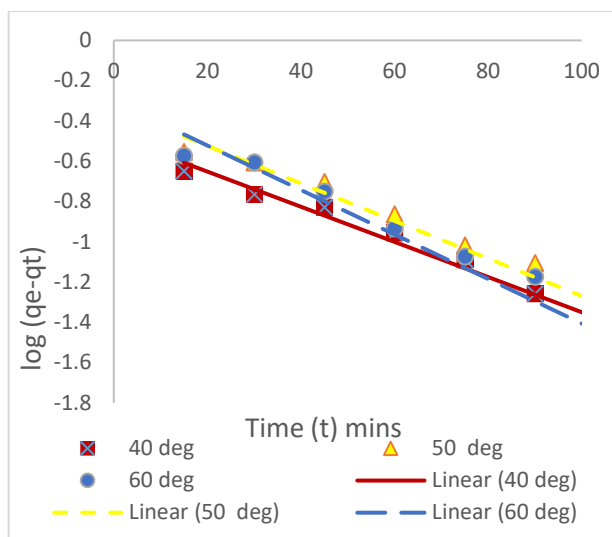


Fig. 3.12 Pseudo-first order kinetics plot of Ln (Qe-Qt) against Time at different temperatures

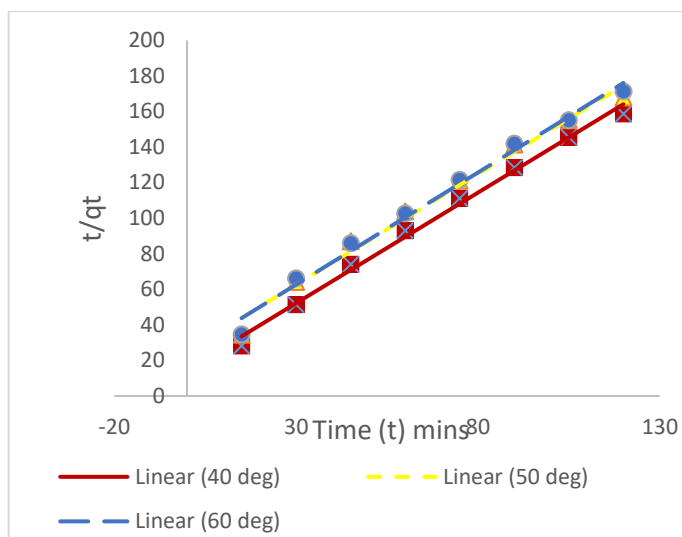


Fig. 3.13 Pseudo-second order plot of T/Q against Time (min) at different temperatures

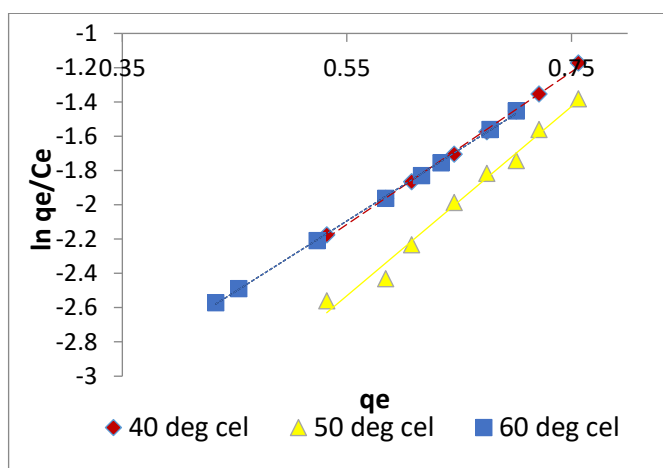


Fig. 3.14 Elovich kinetics model plot of Ln qe/ce against qe at different temperatures

4. CONCLUSION

The biosorption of Bromothymol blue from wastewater onto *G. sepium* and *A. pod* composite has been studied. The biocomposite, *G. sepium* and *A. pod* were modified with 0.1M of diluted Hydrogen peroxide (1: 100) of different mixture ratio of 7 experimental runs as suggested by the design expert software. The most effective run with highest QE and RE is Run 3 (0.95 *G. sepium*: 0.05 *A. pod*). Two-Level factorial design in the Design of Expert was an appropriate tool to evaluate the quality of the model which gave R^2 to be 0.9999 and 0.9851 for adsorption capacity and removal efficiency respectively. The FTIR suggests the surface chemistry of the *G. sepium* and *Acacia* pods, it indicates the large presence of O-H, C-O, N-H and C=C and there was appearance and disappearance of the O-H stretch, C=O, C-Cl, C-F, $c \equiv c$ stretch groups in the unmodified and modified *G. sepium* pod at different peaks, while appearance of C-H, C-Cl, O-H, N-H bend and $c \equiv c$ stretch groups where noticed in the modified and unmodified *A. pod* at different peaks. A decrease in the QE was observed as the biosorbent dose increases while RE was observed to increase as time and dosage increases. QE and RE decreases as temperature increases but increases with time. Pseudo second-order and Elovich models were observed to be suitable as they express the kinetic model well. It can be deduced that *G. sepium* and *A. pod* are effective agricultural materials for the development of a biocomposite as adsorbent in adsorption study due to its high yield, good adsorption capacity, removal efficiency and increase in rate of adsorption.

5. CONFLICT OF INTEREST

There is no conflict of interest associated with this work.

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