

# Log – Periodic Terahertz Antenna with Square Srr Metamaterial Superstrate

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**Abstract**-In this paper a log-periodic terahertz antenna with metamaterial superstrate is proposed. A single-layer metamaterial structure, which utilized as a lens for the enhancement of gain of log-periodic terahertz antenna is used. The proposed metamaterial lens consist of an 8x8 matrix of Square Split-Ring Resonators (SRRs) and is placed above a probe-fed log-periodic terahertz antenna, resonating at 3.8 THz. The simulation result show that the proposed antenna achieves +9.991 dB gain at 4.521 THz, which is about +0.36 dB higher than the maximum gain of the conventional antenna. But proposed antenna provides a maximum gain enhancement of +1.11 dB at 3.846 THz frequency.

**Keywords**- SRRs, THz, Metamaterials, Gain.

## 1. INTRODUCTION

Terahertz (THz) radiation offers many possibilities for new applications in different field because its interesting properties and its special interaction with many materials. The application are radio astronomy, spectroscopy, or civil security. In general the intensity of THz signals is low and the effective detection area of the sensor is very small. In addition there is the difference between free space impedance and detector impedance result in high reflection losses. A bad coupling efficiency is consequence that that makes a detection of THz signals, even for high sensitive detectors like superconducting Hot-Electron Bolometers (HEBs), extremely difficult [1]. One solution to overcome the problems is to use an antenna structure. The use of an antenna result in two main advantages. First, impedance matching of the detector to the free space wave can be achieved over high bandwidth. On the other hand, the effective detection area, that is proportional to the received radiation power, is increased significantly [1].

The appearance of metamaterials open the possibility for RF and microwave engineers to create structures with unconventional properties not found in nature.

The electromagnetic properties of metamaterials can be exploited to enhance the radiation characteristics of antenna [3]. These structures exhibit non-natural behavior, at predefined frequencies, such as very small or even negative permeability values [4].

In the literature, different metamaterials loaded patch antenna are reported to enhance the gain of antenna. The authors of [5] use metamaterials to design a high gain antenna for WiMAX application. There in, a four-layered metamaterial superstrate, consisting of 10x11 periodic array of S-shape resonators, is placed above a rectangular patch. A 1.8 dB gain improvement is attained at resonance

frequency as compared to original antenna. In [6] the metamaterial unit cell is engineered to have zero index of refraction within wide band. The metamaterial surface consists of 7x7 periodic unit cells.

By placing three layers of the proposed metamaterial surface above patch antenna, a 7.8 dB gain improvement is achieved.

In this context, the antenna consisting of a log-periodic structure with a metamaterial inspired superstrate is designed. The proposed metamaterial lens consists of an 8x8 matrix of square split ring resonators (SRRs) of PEC and is positioned above a probe-fed log-periodic terahertz antenna.

## 2. BASIC ANTENNA PRINCIPLES

In comparison to bow-tie or spiral antennas, log-periodic antennas are not real frequency independent antennas. These antennas are based on resonance effects which repeat periodically with the logarithm of the frequency. At a resonance frequency two teeth, which are in symmetry to the center of two adjacent resonance frequencies  $f_n$  and  $f_{n+1}$  depends on the scaling factor  $\tau$ , the inner tooth radius  $r_n$  and outer tooth radius  $R_n$  in this way

$$\frac{f_n}{f_{n+1}} = \frac{R_{n+1}}{R_n} = \frac{r_{n+1}}{r_n} = \sqrt{\tau} \quad (2.1)$$

$$R_n = \tau^{n-0.5} * r_1 \quad (2.2)$$

$$r_n = \tau^{n-1} * r_1 \quad (2.3)$$

The bandwidth of the antenna is limited by the upper and the lower cut-off frequency. The upper cut-off frequency of the antenna is determined by the shortest tooth length. On the other hand, the longest tooth defines the lower cut-off frequency. If the variation of the impedance behavior between two resonances is sufficiently small, the antenna can be assumed as approximately frequency independent [2]. Up to now, two different theories of the principle of operation are present in literature. According to the first theory [7], the log-periodic antenna is considered as a half-wavelength resonator. The resonator consists of two parts: the length of tooth arc with angle  $\alpha$  and the length of a bow-tie segment with angle  $\beta$ . In the second model [8] the teeth are expected to operate as quarter-wavelength resonator with no influence of the bow-tie structure. In the following the log-periodic terahertz antenna type is examined for the half wavelength resonance effect. The lengths of described paths are

$$l_n = r_n (1 + \sqrt{\tau}) * \frac{\alpha\pi}{180^\circ} + r_n (\sqrt{\tau} - 1) \quad (2.4)$$

And hence the corresponding resonance frequencies are

$$f_n = \frac{c_0}{2 \left( r_n (1 + \sqrt{\tau}) * \frac{\alpha\pi}{180^\circ} + r_n (\sqrt{\tau} - 1) \right) \sqrt{\epsilon_{eff}}} \quad (2.5)$$

### 3. METAMATERIAL UNIT CELL CHARACTERIZATION

The metamaterial unit cell shown in fig.3.1 is used as the building block of the beam-focusing substrate. This kind of unit cell is called Split-Ring Resonator (SRR). SRR is formed by a pair of concentric loops with splits at opposite ends.

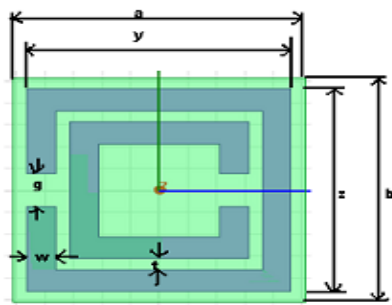


Fig.3.1 A top view of the square SRR metamaterial unit cell

The unit cell strip lines are printed on a Rogers RT/duroid 5880 substrate with relative permittivity  $\epsilon_r = 2.2$ . The square SRR related parameters are shown in table 3.1. Ansoft HFSS, an FEM-based solver is used to calculate the scattering parameters of unit cell [9].

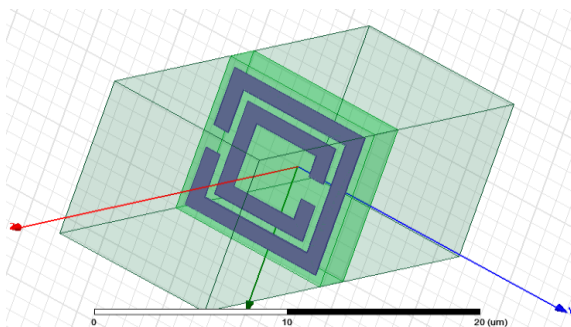


Fig. 3.2 The simulation setup in HFSS for unit cell

The geometrical dimensions of the square SRR, are summarized in table 3.1. The simulated scattering parameters of the unit cell square SRR are shown in fig. 3.3.

TABLE 3.1  
 THE GEOMETRICAL PARAMETERS OF THE SQUARE SRR

a (μm)	b (μm)	y (μm)	z (μm)	g (μm)	w (μm)	t (μm)
10.24	10.24	9.24	9.24	2	2	1

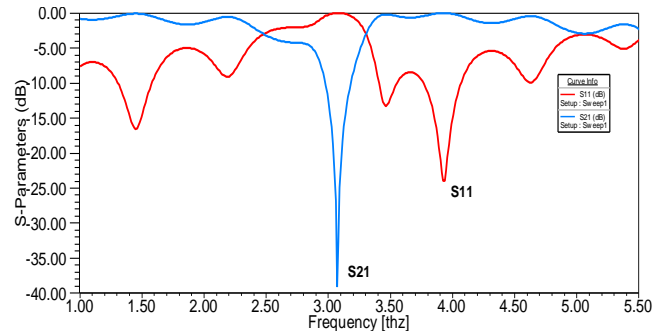


Fig.3.3 The simulated  $S_{11}$  and  $S_{21}$  of the square SRR with respect to frequency

It can be noticed that square SRR has a resonance at 3.8 THz. The normalized permittivity of the SRR, extracted from S-parameters shown in fig.3.4. It can be notice that around 3.8 THz, the permittivity of the structure is negative. Thus, this square SRR constitutes a negative index material medium at the 3.8 THz range.

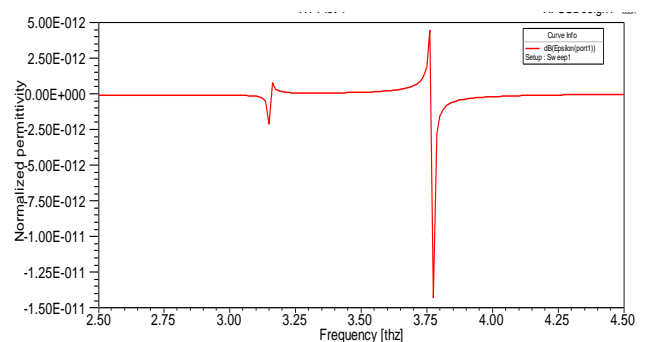


Fig.3.4 The Permittivity of the square SRR.

### 4. ANTENNA DESIGN USING A METAMATERIAL SUPERSTRATE

The SRR, presented in the previous section, is employed as a key building block of a superstrate position above a log-periodic terahertz antenna. The superstrate consist of  $8 \times 8$  periodic array of Square SRRs. These unit cells are separated by  $1 \mu\text{m}$  from each other in both the x and y directions. A  $10 \mu\text{m} \times 10 \mu\text{m}$  blank space at the four superstrate corners is left to provides solid support of the log-periodic terahertz antenna and the superstrate. The space between the radiating patch and the bottom surface of the metamaterial is  $h = 66.5 \mu\text{m}$ . The radiating log-periodic terahertz antenna is printed on a  $100 \mu\text{m} \times 100 \mu\text{m} \times 50 \mu\text{m}$  silicon. The center of the log-periodic terahertz antenna is aligned with that of the supstrate. The top-view of conventional log-periodic terahertz antenna is shown in fig.4.1.

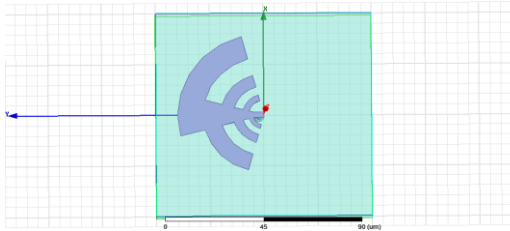


Fig.4.1 The top view of log-periodic terahertz antenna without metamaterial.

TABLE 4.1  
 GEOMETRICAL PARAMETERS OF THE SIMULATED ANTENNA

$r_1$ [ $\mu\text{m}$ ]	$\alpha$ [deg]	$\beta$ [deg]	n	$\tau$
5	60	30	6	$\sqrt{2}$

The 3D view of log-periodic terahertz antenna with square SRR metamaterials is shown in fig.4.2.

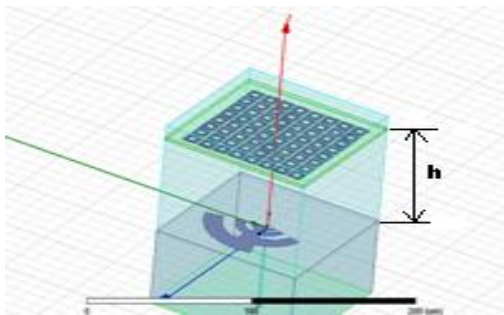


Fig.4.2 The 3D view of Proposed antenna

The height  $h$  of the superstrate is the distance between the log-periodic patch and the metamaterial board, the optimization of height is done using [3]. The probe-fed log-periodic terahertz antenna is designed to operate at frequencies of 2.395 THz, 2.912 THz, 3.385 THz, 3.846 THz and 4.521 THz.

The computed  $S_{11}$  plots of the conventional antenna and proposed antenna is shown in fig.4.3. The presence of the metamaterial does not affect the resonance conditions of original antenna, which is approximately same as an conventional antenna frequencies.

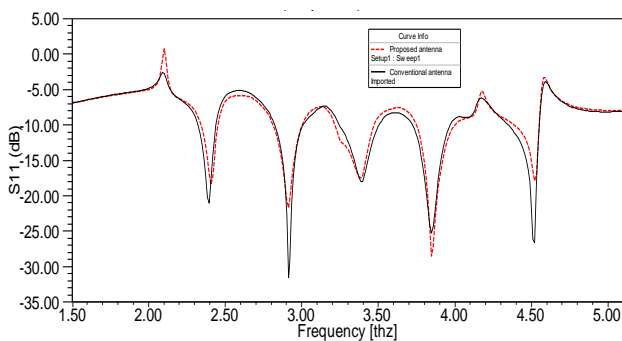


Fig.4.3 The simulated  $S_{11}$  parameters of conventional antenna (continuous line) and proposed antenna (dashed line)

The maximum gain of log-periodic terahertz antenna without metamaterial at 3.846 THz is +0.55 dB, clear from the 3D radiation pattern of the log-periodic terahertz antenna without metamaterial, as shown in fig.4.4.

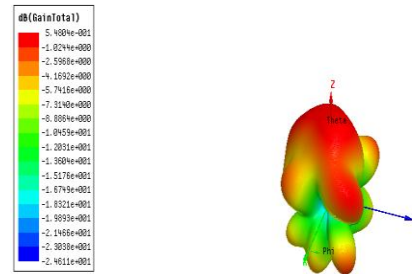


Fig.4.4 3D radiation pattern of log-periodic terahertz antenna without metamaterial

The maximum gain of proposed antenna at 3.846 THz is +1.655, which is approximately 1.11 dB higher than original. The fig.4.5 show the 3D radiation pattern of proposed antenna.

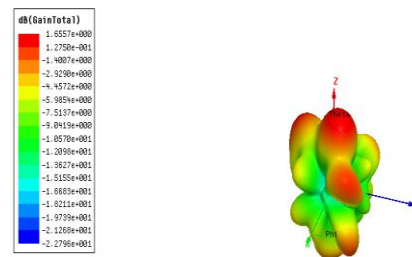


Fig.4.5 The 3D radiation pattern of proposed antenna

Table 4.1 shows the resonance frequency vs gain of log-periodic terahertz antenna and proposed antenna.

S no.	Resonance Freq. (THz)	$S_{11}$ (dB)	Gain Conventional (dB)	Gain Proposed antenna (dB)	Diff. Gain (dB)
1	2.395	-21.0	-2.897	-2.395	+0.50
2	2.912	-31.5	+1.09	+0.901	-0.19
3	3.385	-17.9	-0.815	-0.668	+0.15
4	3.846	-25.3	+0.55	+1.655	+1.11
5	4.521	-26.6	+9.63	+9.991	+0.36

Table 4.1 shows that the gain of proposed antenna are enhance by +0.50 dB, -0.19 dB, +0.15 dB, +1.11 dB and +0.36 dB at frequencies 2.395 THz, 2.912 THz, 3.385 THz, 3.846 THz and 4.521 THz respectively.

The rectangular radiation pattern of both conventional antenna and proposed antenna shown in fig.4.6 (a) and (b). The comparison of pattern shows a decrease in the half-power beamwidth (HPBW) by  $22^\circ$  in the  $\phi = 0^\circ$  plane, and by  $23^\circ$  in the  $\phi = 90^\circ$  with metamaterial superstrate.

TABLE 4.2

THE HPBW OF CONVENTIONAL AND PROPOSED ANTENNA

Antenna type	$\Phi = 0^\circ$ -plane	$\Phi = 90^\circ$ -plane
Conventional	39°	33°
Proposed	17°	10°

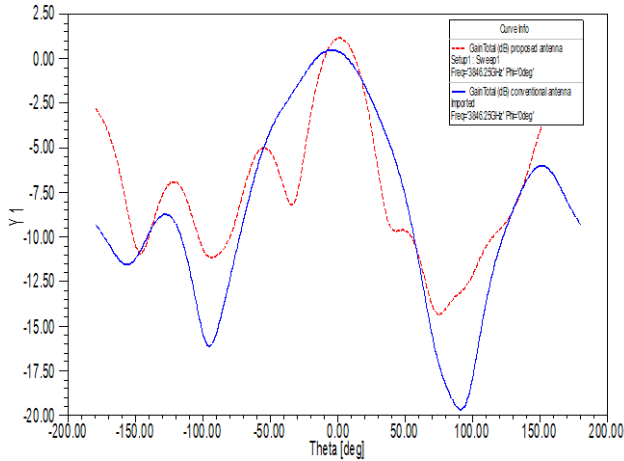


Fig.4.6 (a) The rectangular radiation pattern of conventional antenna (continuous line) and proposed antenna (dashed line) at  $\phi = 0^\circ$ .

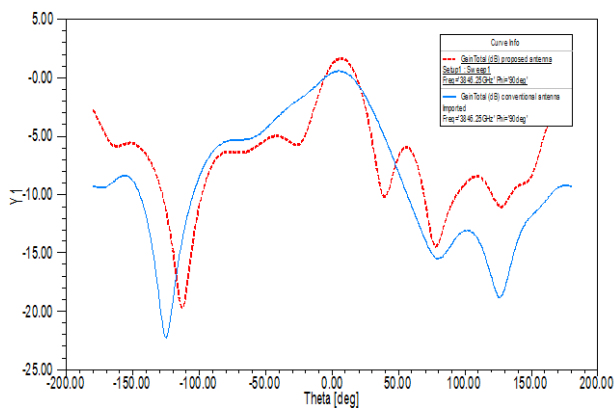


Fig.4.6 (b) The rectangular radiation pattern of conventional antenna (continuous line) and proposed antenna (dashed line) at  $\phi = 90^\circ$ .

### 5. CONCLUSIONS

A log-periodic terahertz antenna with square SRRs metamaterial superstrate is proposed and a single layer metamaterial surface is used as a lens to enhance the gain of log-periodic terahertz antenna. This metamaterial structure is a 2-D array of Square Split-Ring Resonators (SRRs) where effective permittivity is negative at resonance frequency. The lens is positioned above a log-periodic terahertz antenna resonating at 3.8 THz to validate the beam focusing ability. The simulation result shows that the proposed antenna offers a gain improvement of about +1.11 dB at 3.846 THz, in working range of metamaterial superstrate, but it offers a maximum gain of +9.991 dB at 4.521 THz with +0.36 dB gain improvement. Also a considerable decrement in the half-power beamwidth (HPBW) is found, as compared to the conventional antenna.

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