

Stimulation of Dual Tone Multi Frequency Detection Using Bank of Filters

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Abstract

Dual-Tone Multi-frequency (DTMF) techniques have been researched for quite some time and is considered to be the basis for voice communications and is widely used worldwide in modern telephony to dial numbers and configure switchboards. The field has matured enormously over this time, number of procedures, algorithms and testbeds have been built and proposed, several manuscripts have been written, a large number of start-ups have been shaped, and DTMF technology has been deployed in the market place at a very rapid rate. The objective of this paper is to summarize the basic DTMF detection approaches, including Goertzel algorithm which deploys the advantages of Fast Fourier Transform algorithm. Along with it, this paper also presents the computational complexity associated with these algorithms to show cast the importance of Goertzel Algorithm.

1. Introduction

Dual Tone Multi Frequency is a system of signal tones used in the field of communication whose application ranges from voice mail and help desks to telephone banking and controlling robotics designs. There are twelve DTMF signals are made up of two tones from the following selection: 697 Hz, 770 Hz, 852 Hz, 941 Hz, 1209 Hz, 1336 Hz, and 1477 Hz. The tones are divided into low and high groups, and each DTMF signal uses one from each group. This prevents any harmonics from being misinterpreted as part of the signal. The table 1 shows the frequencies used for each signal. The telephones being used at the time of development of DTMF tones were thought to access computers and for this purpose a number of companies were asked to come up with a solution. This led to the addition of the number sign (#, called as 'hash' or 'gate' in the UK) and asterisk or "star"(*) keys as well as a group of keys for menu selection: A, B, C and D. Later, the lettered keys were dropped from most phones before these keys became widely used for vertical service codes like military and government services.

	1209 Hz	1336 Hz	1477 Hz	1633 Hz
697 Hz	1	2	3	A
770 Hz	4	5	6	B
852 Hz	7	8	9	C
941 Hz	*	0	#	D

Table 1. Frequencies used in forming DTMF tones

2. Frequency Detection in Modern Era

Why we need an algorithm for filtering a set of frequencies which could easily be done through using bank of filters? It is because perfect filters are hard to design, implement and achieve. Through this paper we show the complexity involved in filtering the group of frequencies. Another method for filtering small range of frequencies is Goertzel Algorithm. In 1958 Gerald Goertzel came up with his algorithm which utilized the advantages of Fast Fourier Transform (FFT) algorithm but with certain modifications. General FFT algorithm computes evenly across the bandwidth of a given signal but his algorithm looked only at specific, predetermined frequencies. This made his algorithm to work fast for countable number of frequencies. Let's have a look at the algorithm.

2.1. Goertzel Algorithm

The working of Goertzel algorithm is based on equations[1]:

$$Q_n = x(n) + 2\cos\left(\frac{2\pi k}{N}\right) Q_{n-1} - Q_{n-2}$$

$$|y_k(N)| = Q^2(N) + Q^2(N-1) - 2\cos\left(\frac{2\pi k}{N}\right)Q(N)Q(N-1)$$

These equation when implemented lead to Figure 1:

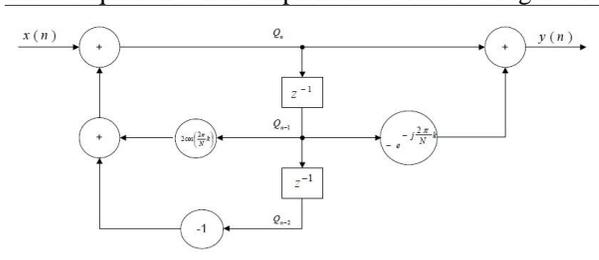


Figure 1. Goertzel Algorithm State Diagram

In the above equation if N is set to 205[1], then the value of k needs to be determined. The value of this constant k also determines the tone we are trying to detect and is given by:

$$k = N * f_{\text{tone}} / f_s$$

Where: f_{tone} = frequency of the tone

f_s = sampling frequency.

Now we can calculate the value of the coefficient and obtain Table 2.

$$2\cos(2\pi k/N)$$

Frequency	K	Coefficient
697	18	1.703275
770	20	1.635585
852	22	1.562297
941	24	1.482867
1209	31	1.163138
1336	34	1.008835
1477	38	0.790074
1633	42	0.559454

Table 2. Calculating the coefficient of the equation

2.2. MATLAB Stimulations

The minimum duration of a DTMF signal prescribed by ITU standard is 40ms. If sampling frequency f_s is taken be 8000 Hz, then 320 samples will be available for estimation and detection. The DTMF decoder needs to estimate the frequencies in these short signals. Computing the Discrete-Time Fourier Transform (DFT) samples for the fundamental tones using 205 samples in the frequency domain minimizes the error between the original frequencies and the estimated points of DFT [1].

Method	Number of Multiplications	Number of Additions
DFT	N^2	$N^2 - (N/2)$
FFT	$(N^2/2) + (N/2)$	$N^2 - N$
Goertzel	$N \log_2(N/2)$	$(3/2)N\log_2(N/2)+4((N/2)-1)$

Table 3. Computational Complexity of algorithms

Hence we keep only 205 samples or 25.6 ms for further processing. At this point we then use the FFT algorithm to calculate DFT. It is here that the popularity of Goertzel algorithm in estimating the DFT for small number of points has proved more efficient than the FFT algorithm.

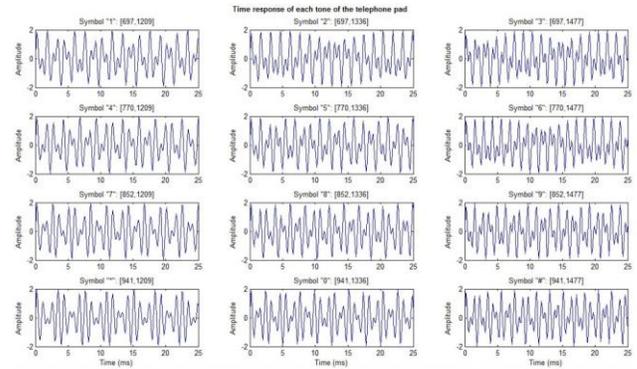


Figure 2. Dual Tone Frequency components of keypads

Table 3 shows the computational complexity comparison between DFT, FFT and Goertzel algorithm. Figure 2 shows the dual tone frequency components of the keypads while Figure 3 shows the Goertzel DFT magnitude estimate of each tone. Latter two stimulations were done on MATLAB and the output obtained is provided.

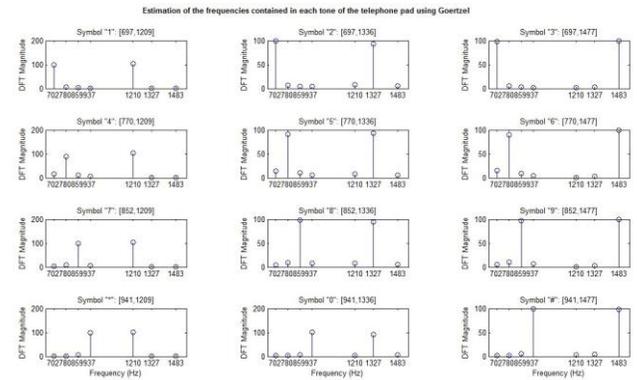


Figure 3. Goertzel DFT magnitude estimate of tones

2.3. Algorithm Used for implementation of Goertzel Algorithm

Here I present the C code based algorithm which is used for the implementation of Goertzel Algorithm. This algorithm can further be programmed in assembly or high level language for hardware implementation of Goertzel Algorithm.

```

Goertzel (double read) \\ declaring function
{
    int delay_1=0; \\ Initialize three
    int delay_2=0; \\ variables with a
    int delay_3=0; \\ value of zero
    int N=0;
    int Goertzel=0;
    int coefficient_1=697; \\ to detect 697 Hz
    int I, product_1,product_2,product_3;
    int sum, output, input;
    double = R_input

    R_input=read; \\ read the input signal
    input = (int) R_input;

    product_1= (delay_2*coefficient_1);
    delay_1=input+product_1-delay_3;
    delay_3=delay_2;
    delay_2=delay_1;
    N++;

    if (N==206)
    {
        product_1=delay_2*delay_2;
        product_2=delay_3*delay_3;
        product_3=delay_2*coefficient_1;
        product_3=product_3*delay_3;
        Goertzel=product_1+product_2-
        product_3;
        N=delay_2=delay_3=0;
    }
    output=(((int)R_input)*Goertzel);
    printf("Value detected is%d",output);
}

```

3. Hardware details and implementation

The complexity of implementing the filtering of small range of frequencies within the prescribed limit of ITU is presented in this paper. The hardware basically deals with band-pass filters bandwidth range lying between 5-25 Hz. To implement this I used Sallen-Key filters used due to the fact that in Sallen Key filters, the op-amp is configured as an amplifier, as opposed to an integrator which minimizes the gain-bandwidth requirement of the op-amp. Along with Sallen-Key filters, two more filters were used of the purpose. These were state-variable filters and Biquad filters. State-variable Q value couldn't be tuned enough so biquad filters were then used as a replacement at certain places. Let's have a look at the basics of these filters and their working.

3.1. Analysis of different filters

Sallen-Key configuration is also known as voltage control voltage source (VCVS), is one the widely used topologies because it's configuration shows least dependence of filter performance of op-amp. In simple words it means that for a given op-amp, higher frequency filter can be designed and the op-amp gain bandwidth product will not limit the performance of the filter when compared to as in integrator. The filter is of non-inverting nature. The component spread, i.e. the ratio between highest component value and lowest component value, is low which is considered good for manufacturability. The Sallen-Key is Q-sensitive to element values which become a serious drawback of this configuration as then it is not easy to tune them due to the interaction and influence of components values on centre frequency.

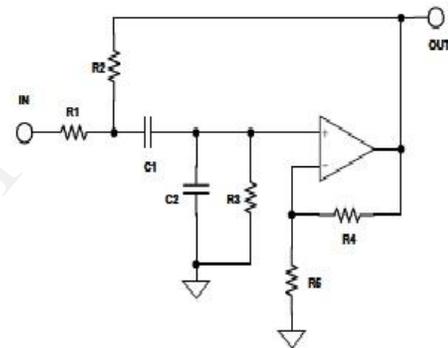


Figure 4. Sallen-Key Band-pass Filters

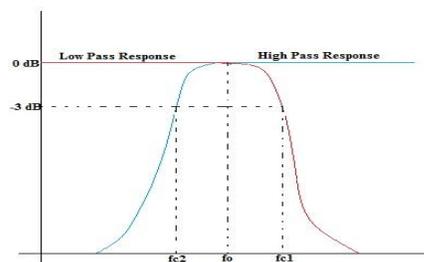


Figure 5. Composite Response curve of second order Sallen-Key filters.

Figure 4 shows the components arrangement in case of Sallen-Key band-pass filters. Their values depend upon the centre frequency. Figure 5 shows the composite curve response of a second order Sallen Key filters. Notice the ideal nature of high pass and low pass filters before the cut off frequencies which has no ripples in pass band.

State-Variable filter offers the best implementation at the expense of more circuit elements. The major

parameters have no effect on each other and are adjusted independently. The low pass, band pass and high pass outputs are available simultaneously but there is a phase shift in case of low pass and high pass outputs while band pass output maintain its phase. Because of the independent adjustment nature of parameters, component spread is also minimized. The added amplifier section sums the low-pass and high-pass output and a notch function come into realization. Figure 6 describe the structure of State-Variable filter and Figure 7 describe the composite response curve of state-variable filters.

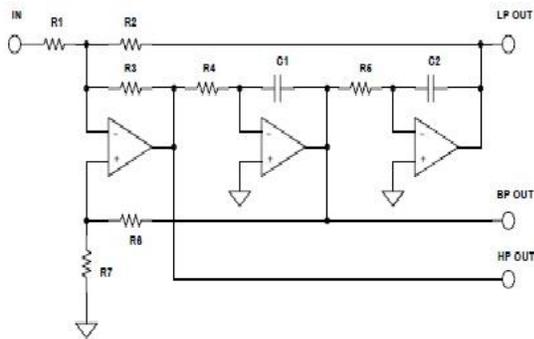


Figure 6. State-Variable Filters

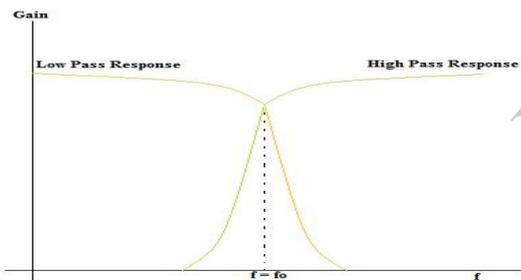


Figure 7. Response curve for State-Variable Filters

Notice the non-ideal nature of high pass and low pass filters and their common cut-off frequency at $f=f_0$. One can infer that the band-pass response actually utilizes the transition band-width of the two filters. The ripples in the low-pass and high-pass region are absent so it may follow the Bessel or Butterworth filter characteristics.

3.2. Important Parameters for Filter Design

Before we look into the working equations used in implementation, certain terms need to be defined. Quality factor (denoted by Q) denotes the selectivity of a band pass filter. The higher the value of Q, the narrower the bandwidth and better the selectivity for a given value of f_0 . Sometimes the band-pass filter are classified as narrow-band and wide-band depending upon the Q value. If Q value is less than 10 it is wide-

band filter and if it is more than 10, it is narrow band filter. Inverse of quality factor is termed as Damping Factor (DF). It determines the filter response characteristics i.e. whether the response will be of Bessel characteristic for Butterworth characteristic. The third and last important parameter of a filter design is the Roll-Off Rate. It is defined as the rate of decrement in gain of a filter below or above the critical frequencies. Higher the roll-off rate, the more we move towards achieving low transition bandwidth. It is also observed that number of poles filter possesses also have an effect on the roll-off rate. Number of poles a filter possesses is defined by the the pairs of resistance and capacitance. It has been observed that higher the number of poles, greater the Roll-off rate.

3.3. Working Equations and Hardware Implementation

The Sallen-Key configuration, for instance, is the least dependent on the frequency response of the amplifier. All that is required is for the amplifier response to be flat to just past the frequency where the attenuation of the filter is below the minimum attenuation required. This is because the amplifier is used as a gain block. Beyond cut-off, the attenuation of the filter is reduced by the roll-off of the gain of the op-amp. This is because the output of the amplifier is phase shifted. There is also an issue with the output impedance of the amplifier rising with frequency as the open loop gain rolls-off. This causes the filter to lose attenuation. It means that the components values needed to design a filter would have to be chosen wisely.

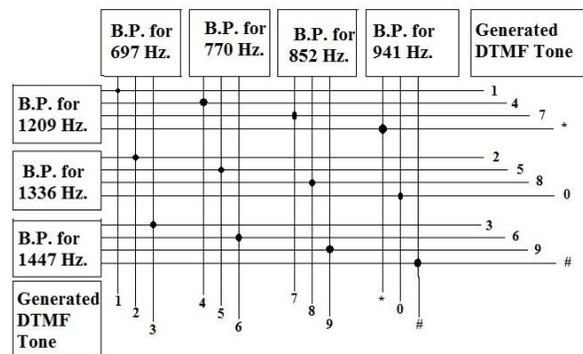


Figure 8. Scheme used for detection of DTMF tones

With the help of 7 filters and 12 logical AND gates we will be able to the DTMF tones. Since the minimum difference between any two pure sinusoidal frequencies is 73 Hz (697 and 770 Hz), the allowed band-width for band-pass filters can range to 25 Hz. A circuit which detect the DTMF of the digit corresponding to '9' is

built using the components and their values are discussed below. It is implemented in MULTISIM and the circuit diagram is given along-side.

The critical frequency of the integrators is given by:

$$f_c = \frac{1}{2\pi R_4 C_1} = \frac{1}{2\pi R_7 C_2}$$

The value of R_4 , R_7 , C_1 and C_2 are those which are mentioned in the State-Variable Filters.

The centre frequency is approximately equal to the critical frequencies of the integrators.

$$f_0 = f_c$$

$$Q = \frac{1}{3} \left(\frac{R_5}{R_6} + 1 \right)$$

$$BandWidth = \frac{f_0}{Q}$$

The Table 4 given below represents the values used in filter design. The values of resistors are given in Ohm and capacitance value is given in Farad.

	R ₁	R ₂	R ₃	R ₄	R ₅	R ₆	C ₁	C ₂
697 Hz	10K	10K	10K	100Ω	200Ω	100Ω	3.3μF	3.3μF
770 Hz	10K	10K	1K	100Ω	200Ω	100Ω	6μF	6μF
852 Hz	10K	10K	1.1K	100Ω	150Ω	400Ω	3.6μF	3.6μF
941 Hz	10K	10K	10K	200Ω	300Ω	150Ω	3.2μF	3.2μF
1209 Hz	10K	10K	1K	150Ω	350Ω	300Ω	2.8μF	2.8μF
1336 Hz	10K	10K	1.1K	300Ω	250Ω	350Ω	2.4μF	2.4μF
1477 Hz	10K	10K	10K	250Ω	200Ω	250Ω	1.6μF	1.6μF

Table 4. Components value used in designing the filters

4. Circuit Simulations

All the stimulations are done on MULTISIM Analog Devices Edition version 10 to neglect the changes due to atmosphere and reduce human error. Figure 9 shows the band-pass configuration for 852 Hz, Figure 10 shows the band-pass configuration for 1477 Hz and Figure 11 shows the combination of these two band-pass configuration for detection of DTMF tone '9'.

Later the different values are also implemented in MULTISIM and then on bread-board to detect the DTMF tones.

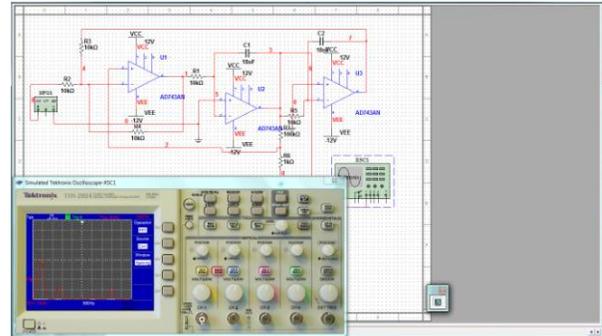


Figure 9. Band-pass configuration for 852 Hz.

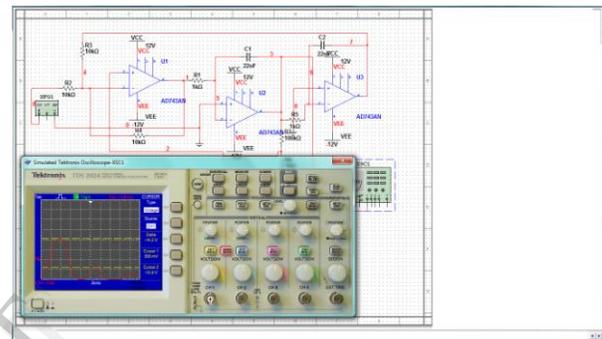


Figure 10. Band-Pass configuration for 1477Hz.

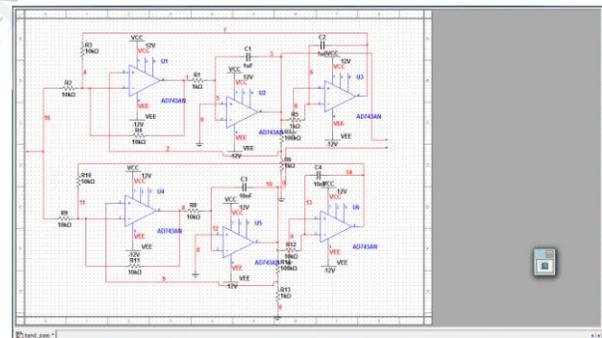


Figure 11. Circuit diagram for Detecting DTMF tone 9.

5. Observations

When a filter is being assembled with components like resistors, capacitors and inductors, tradeoffs must typically be made because the calculated values of components will most likely not be available commercially as they come in standard values. Not only is the cost of components increased, which directly increases the manufacturing cost, but also the loading and tuning of a filter becomes a tedious job if we go to manufacture the filters according to our design, unless we don't have a start-up that meets to the demand of production. Further the tolerance and behaviour over a range of temperatures and time needs to be tracked continuously. As discussed above, the resonant frequency and Q value of a filter are highly

dependent on the components used in the circuit. If the component value due to tolerance and atmospheric conditions starts drifting, the frequency and Q of filter will drift and hence will cause the frequency response to vary. The problem is prominent in case of high order filters. Very low resistance values dissipate a large amount of power. Noise also increases with the square root of resistor values. Larger value of resistors was avoided due to the fact of noise increment and also because it will cause larger offsets due to effects of amplifier bias current.

6. Conclusion

Clearly as depicted in the oscilloscope, the performance obtained from the filters is not upto the mark. The FFT plot in Hanning window is in the prescribed limit, but the sharpness and precision is missing. Goertzel algorithm proves to be a better option to detect the DTMF tones than using the bank of filters.

7. References

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